

INTRODUCTION  
TO  
GENERAL AND MEAN-FIELD  
DYNAMO THEORY

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1. Cosmic magnetic fields and the question of their origin
2. The idea of the self-exciting dynamo
3. Elements of magnetofluidynamics
4. The kinematic dynamo problem
5. The general dynamo problem
6. Mean-field electrodynamics
7. Mean-field magnetofluidynamics
8. Kinematic mean-field dynamo models

1.

# COSMIC MAGNETIC FIELDS

## AND THE QUESTION OF THEIR ORIGIN

Table 1. Magnetic fields of various cosmic objects and their spatial extents. All values of the magnetic flux densities and the linear dimensions of the objects have to be understood as orders of magnitude only.

Object	Magnetic flux density [ T ]	Linear dimension of the object [ m ]	Symmetry and time behaviour of the magnetic field
Earth	$10^{-4}$	$10^7$ ( $10^4$ km)	slight deviations from symmetry about rotation axis and equatorial plane, non-oscillatory, reversals
Planets	$10^{-8} \dots 10^{-3}$	$10^6 \dots 10^8$ ( $10^3 \dots 10^5$ km)	various degrees of symmetry
Sun	some $10^{-1}$ (in spots)	$10^9$ ( $10^6$ km)	slight deviations from symmetry about rotation axis and equatorial plane oscillatory, magnetic cycle, grand minima
Cool stars (F, G)		$10^9$ ( $10^6$ km)	sun-like magnetic cycles
Hot stars (A, B)	1	$10^9$ ( $10^6$ km)	oblique rotators
White dwarfs	$10^4$	$10^5$ (100 km)	
Neutron stars	$10^8$	$10^4$ (10 km)	oblique rotators
Galaxies	$10^{-9}$	$10^{21}$ (30 kpc)	"axisymmetric" and "bisymmetric" structures

Suggestions  
concerning the origin  
of cosmic magnetic fields

$$\nabla \times H = j$$

$$\nabla \cdot B = 0$$

- Permanently magnetized matter  
ferromagnetism  
Curie-temperature  $< 1000^\circ\text{C}$

$$j = 0$$

$$B = \mu_0(H + M)$$

- Electric currents

- relic currents / fields

$$\text{decay time } \tau = \mu_0 \sigma L^2$$

Earth:  $10^9$  yrs

Sun-like bodies:  $\approx$  age of the universe

$$j = \sigma E =$$

$$B = \mu_0 H$$

- currents driven by electromotive forces  
independent of electromagnetic fields,

e.g.,

- chemical inhomogeneities
- chemical and temperature inhomogeneities (Seebeck-effect)
- Nichols-Tolman-effect

$$j = \sigma(E + E^{(c)})$$

$$B = \mu_0 H$$

⋮

- currents driven by fluid motions  
in a magnetic field

DYNAMO

$$j = \sigma(E + u \times B)$$

$$B = \mu_0 H$$

● 2.

## THE IDEA OF THE SELF-EXCITING DYNAMO

Sir Joseph Larmor 1919

How Could a Rotating Body such as the Sun  
Become a Magnet ?

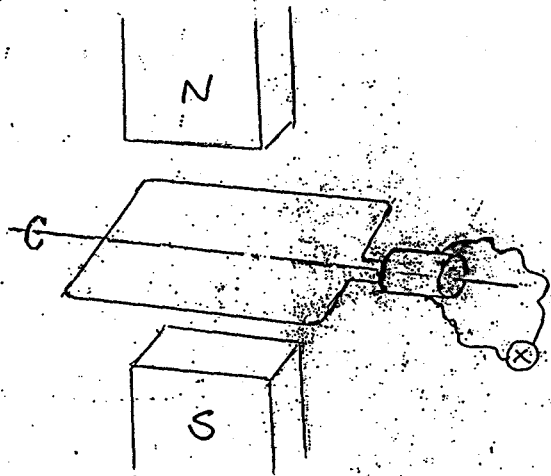
Rep. 87th Meeting Brit. Assoc. Adv. Sci.  
Bournemouth 1919, Sept. 9 - 13,  
John Murray London, pp 159 - 160

... internal motion induces an electrical field  
acting on the moving matter ...

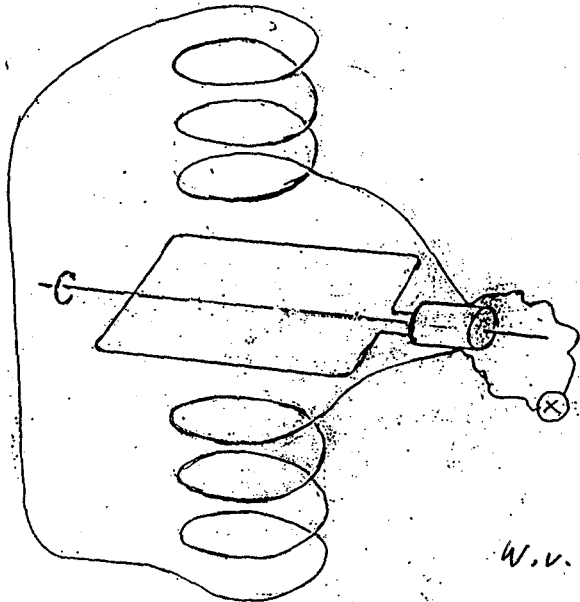
... if a conducting path ... happens to be open,  
an electric current will flow round it,  
which may in turn increase the inducing magnetic field.

In this way it is possible for the internal cyclic motion  
to act after the manner  
of the cycle of a self - exciting dynamo,  
and maintain a permanent magnetic field  
from insignificant beginnings,  
at the expense of some of the energy  
of the internal circulation.

... earth's magnetic field ...  
... it would require fluidity and residual circulation  
in deepseated regions.



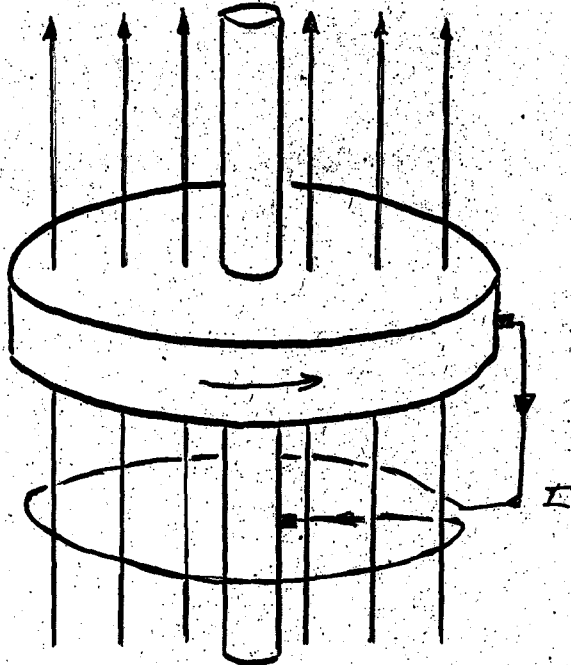
EXTERNALLY  
EXCITED  
DYNAMO



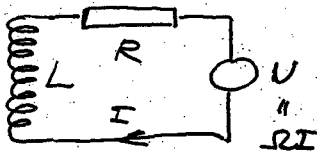
SELF-  
EXCITING  
DYNAMO

W.v. Siemens 1867  
(1857?)  
Ch. Wheatstone 1867

# DISK DYNAMO



angular velocity  $\Omega$



$$L\dot{I} + RI = \Omega I$$

$\leadsto$

$$L\dot{I} + (R - \Omega)I = 0$$

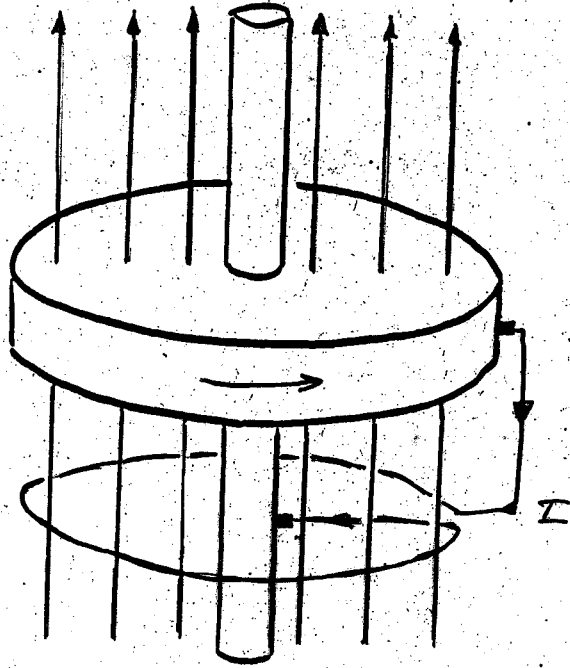
$\leadsto$

$$I(t) = I(0) \exp\left(-\frac{R - \Omega}{L} t\right)$$

$R > \Omega$  DECAY

$R \leq \Omega$  DYNAMO

# DISK DYNAMO

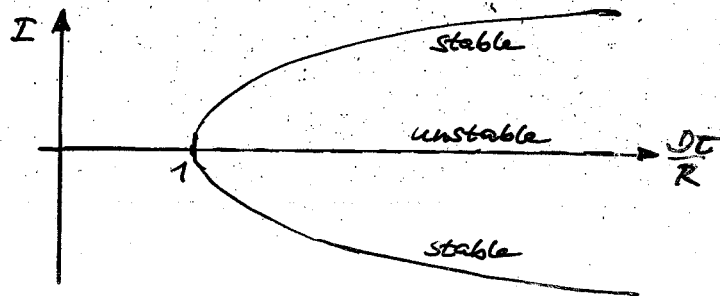


torque  $D$

$$L\dot{I} + (R - \Omega)I = 0$$

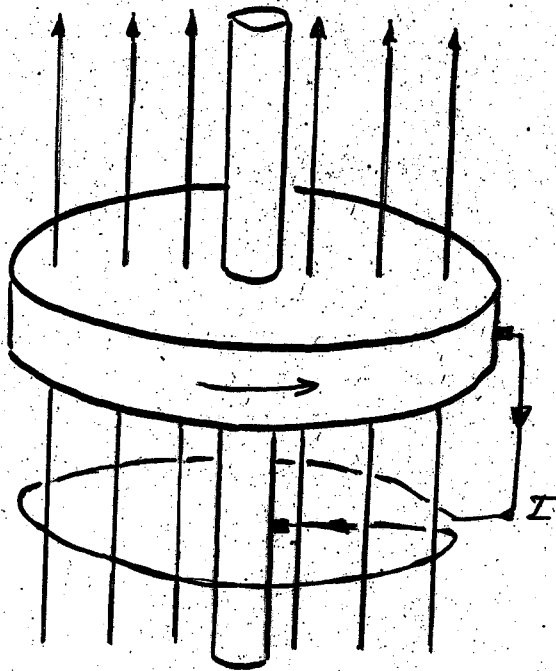
$$\dot{\Omega} + \frac{1}{\tau} \Omega = \frac{D}{\tau + CI^2}$$

Steady states  $\dot{I} = \dot{\Omega} = 0$





# DISK DYNAMO

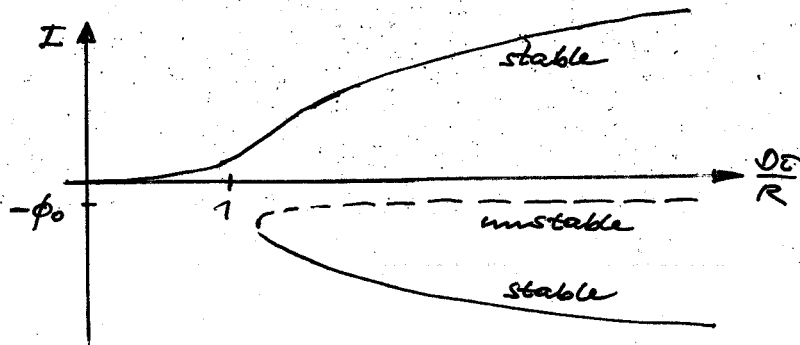


torque  $\mathcal{D}$

$$L \dot{I} + (R - \Omega) I = \Omega \phi_0 \leftarrow \text{imposed magnetic field}$$

$$\dot{\Omega} + \frac{1}{\tau} \Omega = \frac{\mathcal{D}}{1 + cI^2}$$

Steady cases  $\dot{I} = \dot{\Omega} = 0$



• 3.

## ELEMENTS OF MAGNETOFLUIDDYNAMICS

• 3.1.

Maxwell equations and constitutive equations in the magnetofluiddynamic approximation

- flat space
- high electric conductivity  
 $\epsilon_0 / \sigma \ll T$   $T$  characteristic time of the considered process
- non-relativistic velocities  
 $(u/c)^2$  negligible in comparison to 1

$$\nabla \times E = -\partial_t B \quad \text{Faraday's law}$$

$$\nabla \cdot B = 0$$

$$\nabla \times H = j \quad \text{Ampere's law}$$

$$B = \mu H$$

$$j = \sigma (E + u \times B) \quad \text{Ohm's law}$$

$\nearrow$  Lorentz e.m.f.  $+ E^{(e)}$  external e.m.f.

international system of units  
(m, kg, s, V, A, ...)

- approximations!

$$\left[ \begin{array}{l} \nabla \cdot D = \rho_{ex} \\ D = D(E, B) \end{array} \right] \text{ - of secondary interest}$$

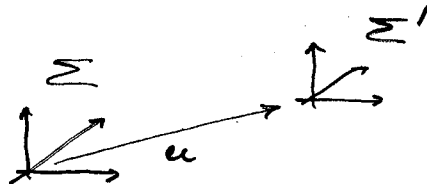
Transformation laws

$$B' = B$$

$$H' = H$$

$$j' = j$$

$$E' = E + u \times B$$



• 3.2.

Induction equation

$$\nabla \times (\eta \nabla \times \mathbf{B} - \mathbf{u} \times \mathbf{B}) + \frac{\partial \mathbf{B}}{\partial t} = 0 + \nabla \times \mathbf{E}^{(e)}$$

$$\nabla \cdot \mathbf{B} = 0 \quad \eta = 1/\mu\sigma \text{ magnetic diffusivity}$$

$$\eta = \text{const} \leadsto$$

$$\eta \nabla^2 \mathbf{B} + \nabla \times (\mathbf{u} \times \mathbf{B}) - \frac{\partial \mathbf{B}}{\partial t} = 0 - \nabla \times \mathbf{E}^{(e)}$$

Advection/diffusion ratio:

$$\frac{|\mathbf{u} \times \mathbf{B}|}{|\eta \nabla \times \mathbf{B}|} = \frac{UL}{\eta_c} \quad \begin{array}{l} U \text{ characteristic value of } |\mathbf{u}| \\ L \text{ characteristic length scale} \\ \eta_c \text{ characteristic value of } \eta \end{array}$$

$$R_m = \frac{UL}{\eta_c} \text{ magnetic Reynolds number}$$

$R_m \ll 1$  diffusion-dominated processes

$R_m \gg 1$  advection-dominated processes

Time scales

$$T_\eta = L^2/\eta_c \text{ diffusive time scale}$$

$$T_u = L/U \text{ kinetic time scale}$$

Dimensionless variables

$$x \rightarrow Lx \quad t \rightarrow tT \quad \mathbf{u} \rightarrow uU \quad \eta = \tilde{\eta}\eta_c$$

$$T = T_\eta \leadsto \nabla \times (\tilde{\eta} \nabla \times \mathbf{B} - R_m \mathbf{u} \times \mathbf{B}) + \frac{\partial \mathbf{B}}{\partial t} = 0$$

$$T = T_u \leadsto R_m^{-1} \nabla \times (\tilde{\eta} \nabla \times \mathbf{B}) - \nabla \times (\mathbf{u} \times \mathbf{B}) - \frac{\partial \mathbf{B}}{\partial t} = 0$$

Table 2. Values of the magnetic Reynolds number  $R_m$  and the diffusion and kinematic times  $T_\eta$  and  $T_u$  for laboratory devices as well as the Earth and the Sun. As a comparison value for the electric conductivities  $\sigma$  we note that for copper:  $6 \cdot 10^7$  S/m. For the laboratory devices  $U$  and  $L$  are arbitrarily chosen. For the Earth's core  $U$  gives a plausible magnitude of the internal motion, and  $L$  corresponds to about one third of the radius. As far as the the convection zone of the Sun is concerned, for granules  $U$  and  $L$  give their typical scales at the surface, and for sunspots  $L$  reflects their typical horizontal extension at the surface. For the consideration concerning the interior of the Sun,  $L$  is taken as roughly one third of the solar radius. More comments concerning the values for the Earth's core and the Sun's interior are given in Section 3.4, and concerning the values for the Sun's convection zone in Section 5.7.

	$\sigma$ [ S/m ] $\eta$ [ m <sup>2</sup> /s ]	$U$ [ m/s ]	$L$ [ m ]	$R_m$	$T_\eta$ [ s ]	$T_u$ [ s ]
Mercury 18°C	$1.04 \cdot 10^6$ $7.65 \cdot 10^{-1}$	1	1	1.3	1.3	1
Sodium 100°C	$1.03 \cdot 10^7$ $7.73 \cdot 10^{-2}$	1	1	12.9	12.9	1
Earth's core	$3 \cdot 10^5$ 2.65	$10^{-3}$	$10^6$	$3.8 \cdot 10^2$	$3.8 \cdot 10^{11}$ ( $1.2 \cdot 10^4$ yrs)	$10^9$ (32 yrs)
Sun's convection zone	$3 \cdot 10^3$ $2.65 \cdot 10^2$					
granules		$2 \cdot 10^2$	$2 \cdot 10^6$	$1.5 \cdot 10^6$	$1.5 \cdot 10^{10}$ ( $4.8 \cdot 10^2$ yrs)	$10^4$ (2.8 h)
sunspots			$10^7$		$3.8 \cdot 10^{11}$ ( $1.2 \cdot 10^4$ yrs)	
Sun's interior	$10^8$ $8.0 \cdot 10^{-3}$		$2 \cdot 10^8$		$5.0 \cdot 10^{18}$ ( $1.6 \cdot 10^{11}$ yrs)	

● 3.3.

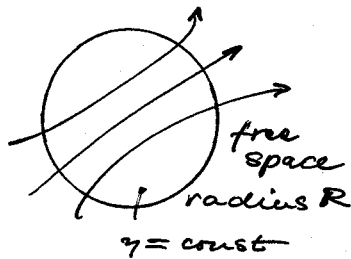
The case  $R_m = 0$

$$\nabla \times (\eta \nabla \times \mathbf{B}) + \partial_t \mathbf{B} = 0$$

$$\nabla \cdot \mathbf{B} = 0$$

Magnetic fields are bound to decay.

Free decay of a magnetic field  
penetrating a spherical conductor



modes

$$\mathbf{B}(\mathbf{x}, t) = \hat{\mathbf{B}}(\mathbf{x}) e^{-\lambda t}$$

slowest-decaying mode  
is a dipole field

with

$$\lambda = \pi^2 \eta / R^2$$

$$T_{\text{decay}} = R^2 / \pi^2 \eta$$

Earth's core

$$R = 3 \cdot 10^6 \text{ m}$$

$$\sigma = 3 \cdot 10^5 \text{ S/m}$$

$$\eta = 2.65 \text{ m}^2/\text{s}$$

$$\Rightarrow T_{\text{decay}} = 1.1 \cdot 10^6 \text{ yrs}$$

Sun-like body

$$R = 7 \cdot 10^8 \text{ m}$$


$$\sigma = 10^8 \text{ S/m}$$

$$\eta = 8 \cdot 10^{-3} \text{ m}^2/\text{s}$$

$$\Rightarrow T_{\text{decay}} = 2 \cdot 10^{11} \text{ yrs}$$

• 3.4.

Magnetic flux

$$\Phi_m = \int_{\mathcal{P}} \mathbf{B} \cdot d\mathbf{s}$$


$\Phi_m$  is the same  
for all surfaces  
coinciding in  $\partial\mathcal{P}$

Time variation

of the magnetic flux through a material surface  
(i.e., a surface moving with the fluid)

$$\frac{d\Phi_m}{dt} = \int_{\mathcal{P}} \left( \frac{\partial \mathbf{B}}{\partial t} - \nabla \times (\mathbf{u} \times \mathbf{B}) \right) \cdot d\mathbf{s} = - \int_{\partial\mathcal{P}} \frac{\mathbf{j}}{\sigma} \cdot d\mathbf{l}$$

$$- \nabla \times (\mathbf{E} + \mathbf{u} \times \mathbf{B})$$

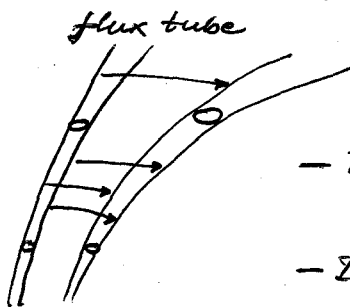
$\mathbf{j}/\sigma$

•

The high-conductivity limit  $R_m \rightarrow \infty$

$$\left. \begin{aligned} \frac{\partial \mathbf{B}}{\partial t} - \nabla \times (\mathbf{u} \times \mathbf{B}) &= 0 \\ \frac{d\Phi_m}{dt} &= 0 \end{aligned} \right\} \begin{array}{l} \text{equivalent} \\ \text{to each other} \end{array}$$

○ Frozen-in magnetic field lines



-  $\Phi_m$  coincides for all cross-sections  
of a given flux tube

- The fluid flow transform a flux tube  
again in a flux tube.

- If, at a given time, two fluid elements  
are connected by a field line  
they are always connected by a field  
line.

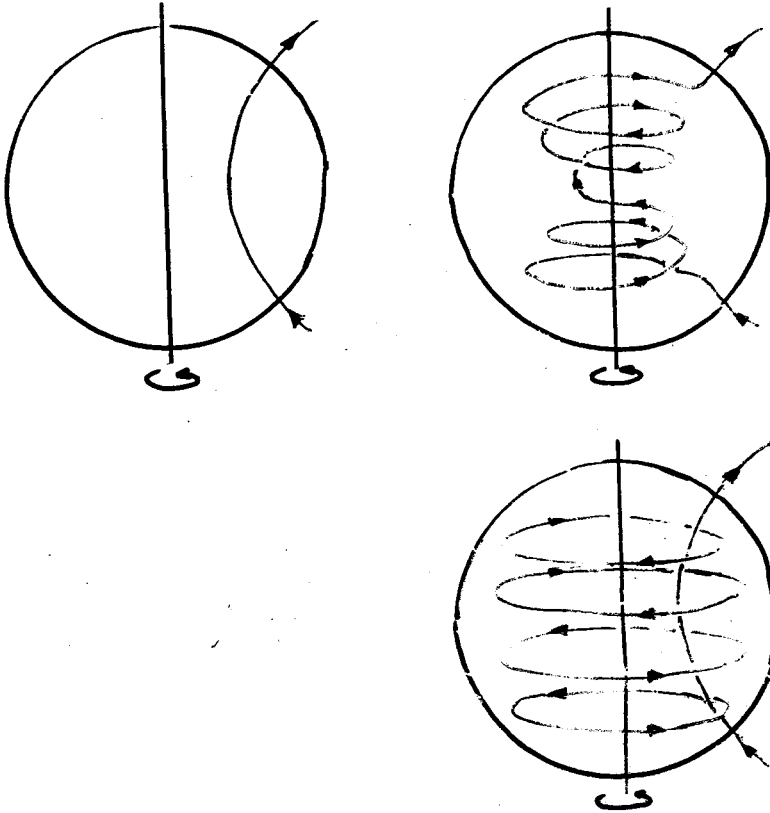
● 3.5.

Advection of magnetic fields

○ 3.5.1.

Differential rotation

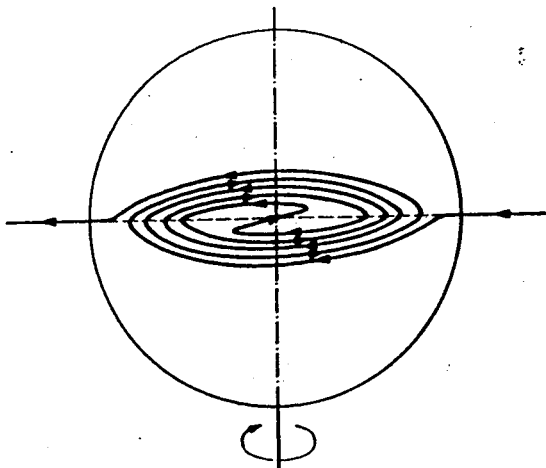
and axisymmetric magnetic field



○ 3.5.2.

Differential rotation

and non-axisymmetric magnetic field



• 3.6.

Magnetic energy

$$\frac{\partial}{\partial t} \left( \frac{B^2}{2\mu} \right) = -\mathbf{j} \cdot \mathbf{E} - \text{div} \mathbf{S} \quad \mathbf{S} = \mathbf{E} \times \mathbf{H}$$

Poynting vector

$$= -\frac{\mathbf{j}^2}{\sigma} - \underbrace{\mathbf{u} \cdot (\mathbf{j} \times \mathbf{B})}_{\substack{\text{work done by Lorentz force (if } > 0) \\ \text{or against it (if } < 0)}} - \text{div} \mathbf{S}$$

Joule heat production

conducting body  $\mathcal{V}$

outer space

$$\mathbf{E} = O(r^{-2}), \quad \mathbf{H} = O(r^{-3})$$

$$\frac{d}{dt} \underbrace{\int_{\infty} \frac{B^2}{2\mu} dv}_{\substack{\text{total} \\ \text{magnetic energy}}} = - \int_{\mathcal{V}} \frac{\mathbf{j}^2}{\sigma} dv - \int_{\mathcal{V}} \mathbf{u} \cdot (\mathbf{j} \times \mathbf{B}) dv$$

$$- \int_{\mathcal{V}} \mathbf{u} \cdot (\mathbf{j} \times \mathbf{B}) dv$$

$$= \frac{1}{\mu} \int_{\mathcal{V}} \left( e_{ij} - \frac{1}{2} (\nabla \cdot \mathbf{u}) \delta_{ij} \right) B_i B_j dv - \frac{1}{\mu} \int_{\partial \mathcal{V}} (\mathbf{u} \cdot \mathbf{B}) (\mathbf{B} \cdot d\mathbf{s})$$

$$e_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \text{ rate of strain tensor}$$

Growth of total magnetic energy

requires stretching of magnetic field lines



● 3.7.

Fluid dynamic equations

Rotating frame of reference,  
angular velocity  $\Omega$

$$\rho(\partial_t u + (u \cdot \nabla)u) = -\nabla p - 2\rho\Omega \times u \leftarrow \begin{array}{l} \text{momentum} \\ \text{balance} \end{array}$$

$+ F^{(fr)} + F^{(ext)} + F^{(em)}$   
 pressure, centrifugal term included    frictional force    external force    electromagnetic force

$$\partial_t \rho + \nabla \cdot (\rho u) = 0 \quad \leftarrow \begin{array}{l} \text{mass} \\ \text{balance} \end{array}$$

$$\rho = \rho(p, T) \quad \leftarrow \begin{array}{l} \text{equation} \\ \text{of state} \end{array}$$

$$\rho c_v (\partial_t T + u \cdot \nabla T) = \nabla \cdot (\tilde{\kappa} \nabla T) - q \quad \leftarrow \begin{array}{l} \text{heat transport} \\ \text{equation} \end{array}$$

specific heat capacity    heat conduction coefficient    heat production

$$F_i^{(fr)} = \frac{\partial S_{ij}}{\partial x_j}$$

$$S_{ij} = \rho \nu \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + \rho \nu' (\nabla \cdot u) \delta_{ij}$$

kinematic viscosity

$$q = \dots (\text{external heating, viscos and Joule heating})$$

• 3.2.

Lorentz force

$$F^{(elem)} \stackrel{\text{magnetofluiddynamic approximation}}{=} F_L \quad (\text{see } E \text{ ignored})$$

Lorentz force

$$= \mathbf{j} \times \mathbf{B}$$

$$= \frac{1}{\mu} (\nabla \times \mathbf{B}) \times \mathbf{B}$$

$$= \frac{1}{\mu} (\mathbf{B} \cdot \nabla) \mathbf{B} - \frac{1}{2\mu} \nabla B^2$$

tension      pressure force

$$F_{Li} = \frac{\partial M_{ij}}{\partial x_j}, \quad M_{ij} = \frac{1}{\mu} (\mathbf{B}_i \mathbf{B}_j - \frac{1}{2} B^2 \delta_{ij})$$

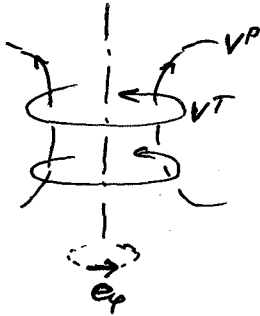
Maxwell stresses

• 3.9.

A useful mathematical tool:  
poloidal and toroidal vector fields

○ 3.9.1.

Axisymmetric case



$$V = V^P + V^T$$

$$V^P = V - (V \cdot e_\phi) e_\phi \quad \text{POLOIDAL}$$

$$V^T = (V \cdot e_\phi) e_\phi \quad \text{TOROIDAL}$$

E.g., spherical coordinate system  
( $r, \theta, \phi$ )

$$V^P = (V_r, V_\theta, 0)$$

$$V^T = (0, 0, V_\phi)$$

•  $V=0 \Leftrightarrow V^P = V^T = 0$

•  $f V^P$  poloidal,  $f V^T$  toroidal  
    *f any scalar*

•  $r \times V^P$  toroidal,  $r \times V^T$  poloidal  
    *r any poloidal vector, e.g., radius vector*

•  $\nabla \cdot V^T = 0$

•  $\nabla \times V^P$  toroidal,  $\nabla \times V^T$  poloidal

$\nabla^2 V^P$  poloidal  
     $\nabla^2 V^T$  toroidal

•  $\nabla \times V^T = 0 \Leftrightarrow V^T = 0$

•  $V^P \cdot V^T = 0$

Special case  $\nabla \cdot V = 0 \Leftrightarrow \nabla \cdot V^P = 0$

$$V^P = \nabla \times \hat{V}^T$$

o 3.9.2.

General case

$$V = V^P + V^T \quad \text{not } |V|$$

$$V^P = rV + \nabla W \quad \text{POLOIDAL}$$

$$V^T = r \times \nabla U \quad \text{TOROIDAL}$$

$r$  radius vector

Spherical coordinate system  $(r, \vartheta, \varphi)$

$$V^P = \left( rV + \frac{\partial W}{\partial r}, \frac{1}{r} \frac{\partial W}{\partial \vartheta}, \frac{1}{r \sin \vartheta} \frac{\partial W}{\partial \varphi} \right)$$

$$V^T = \left( 0, -\frac{1}{\sin \vartheta} \frac{\partial U}{\partial \varphi}, \frac{\partial U}{\partial \vartheta} \right)$$

•  $V = 0$  on  $r = \text{const}$   $\Leftrightarrow V^P = V^T = 0$  on  $r = \text{const}$

•  $f V^P$  poloidal,  $f V^T$  toroidal

if  $f$  independent of  $\vartheta$  and  $\varphi$

•  $r \times V^P$  toroidal,  $r \times V^T$  poloidal

if  $r$  radius vector

•  $\nabla \cdot V^T = 0$  }  $\nabla^2 V^P$  poloidal

•  $\nabla \times V^P$  toroidal,  $\nabla \times V^T$  poloidal }  $\nabla^2 V^T$  toroidal

•  $r \cdot (\nabla \times V^T) = 0$  on  $r = \text{const}$   $\Leftrightarrow V^T = 0$  on  $r = \text{const}$

•  $\langle V^P \cdot V^T \rangle = 0$ , where  $\langle \dots \rangle$  average over  $r = \text{const}$

Special case  $\nabla \cdot V = 0 \quad \Leftrightarrow \nabla \cdot V^P = 0$

$$V^P = \nabla \times (r \times \nabla U)$$

$$V^T = r \times \nabla U$$

o 3.9.3

Applications to  $B$

$$B = B^P + B^T$$

- Axisymmetric case

$$B^P = \nabla \times (A e_\varphi) = -\frac{1}{r \sin \vartheta} \nabla (r \sin \vartheta A)$$

$$B^T = B e_\varphi \text{ with } |B|$$

$r \sin \vartheta A(r_0, \vartheta_0)$  magnetic flux  
through circle  $r = r_0, \vartheta = \vartheta_0$

$r \sin \vartheta A(r, \vartheta) = \text{const}$  defines  
poloidal field lines

- General case

$$B^P = -\nabla \times (r \times \nabla S) = -r \Delta S + \nabla \frac{\partial}{\partial r} (rS)$$

$$B^T = -r \times \nabla T$$

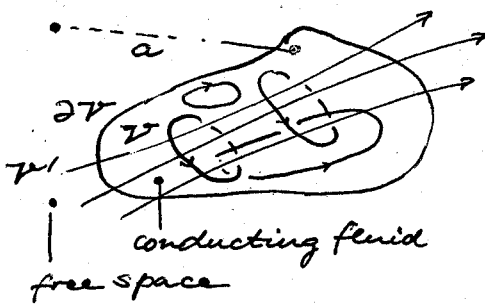
$T = \text{const}, r = \text{const}$  defines  
toroidal field lines

• 4.

THE KINEMATIC DYNAMO PROBLEM

• 4.1.

Formulation of a typical problem



magnetic field  
flux density  $B$   
electric current  
current density  $j$   
fluid motion  
velocity  $u$

(I)  $\nabla \times E = -\frac{\partial B}{\partial t}$  } Faraday's Law  
 $\nabla \times H = j$  } every-where Ampere's Law  
 $\nabla \cdot B = 0$  } initial condition only  
 $B = \mu H$  }  
 $j = \begin{cases} \sigma(E + u \times B) & \text{in } V \\ 0 & \text{in } V' \end{cases}$  } Ohm's Law  
 $E = O(a^{-2})$  } no electric charges  
 $B = O(a^{-3})$  as  $a \rightarrow \infty$  } or currents at infinity

(II)  $\nabla \times (\eta \nabla \times B - u \times B) + \frac{\partial B}{\partial t} = 0$  } in  $V$   
 $\nabla \cdot B = 0$  }  $\eta = 1/\mu\sigma$   
 $\nabla \times B = 0$  } in  $V'$  } If  $V'$  simply connected.  
 $\nabla \cdot B = 0$  } }  $B = -\nabla \phi$  } in  $V'$   
 $\Delta \phi = 0$  } }  
 $[B] = 0$  across  $\partial V$  } no surface currents  
 $B = O(a^{-3})$  as  $a \rightarrow \infty$

Initial value problem for  $B(x,t)$

(I) and (II) (almost) equivalent.

DYNAMO:  $B \rightarrow 0$  as  $t \rightarrow \infty$

$\nabla \times B = 0$  in  $V'$   
and  
 $[B] = 0$  across  $\partial V$   
imply  
 $(\nabla \times B)_n = 0$  at  $\partial V$

• 4.2.

Some comments

$$R_{m} = \frac{UL}{\eta c}$$

o 4.2.1

Necessary (but not sufficient) for a dynamo:

$$R_m \geq R_{m, \text{crit}} = O(1)$$

o 4.2.2

» Dynamo « means more than amplification of magnetic fields

$$\nabla \times (\eta \nabla \mathbf{B} - \mathbf{u} \times \mathbf{B}) + \frac{\partial \mathbf{B}}{\partial t} = \nabla \times \mathbf{E}^{(e)}$$

DYNAMO: non-decaying solution of the homogeneous equation

o 4.2.3

A dynamo corresponds to an instability of the non-magnetic state of a system

Consider problem (II) with  $\mathbf{u}$  independent of  $t$  and look for solutions of the form

$$\mathbf{B}(\mathbf{x}, t) = \text{Re} (\hat{\mathbf{B}}(\mathbf{x}) \exp\{pt\}) \quad \hat{\mathbf{B}}, p \text{ complex}$$

$$\nabla \times (\eta \nabla \times \hat{\mathbf{B}} - R_m \mathbf{u} \times \hat{\mathbf{B}}) + p \hat{\mathbf{B}} = 0$$

etc.

Eigenvalue problem for  $p$

$$p = p(R_m)$$

$$p = \lambda + i\omega \quad \lambda, \omega \text{ real}$$

$$\text{DYNAMO: } \underline{\lambda \geq 0}$$

$\lambda = 0$  defines »marginal values« of  $R_m$

In general infinite set of solutions:  $\hat{\mathbf{B}}_i, p_i$

If set of  $\hat{\mathbf{B}}_i$  complete then general solution of the initial value problem

$$\mathbf{B}(\mathbf{x}, t) = \text{Re} \left( \sum_i c_i \hat{\mathbf{B}}_i(\mathbf{x}) \exp\{pt\} \right)$$

↑ constants determined by  $\mathbf{B}(\mathbf{x}, 0)$

o 4.2.4

Reduction of problem ( $\Pi$ ) (for all space)  
to an »inner problem« (for the fluid body)

Suppose  $V'$  simply connected so that

$$\left. \begin{array}{l} \mathbf{B} = -\nabla\phi \\ \Delta\phi = 0 \\ -\mathbf{n}\cdot\nabla\phi = B_n \text{ on } \partial V \end{array} \right\} \begin{array}{l} \text{in } V' \\ \text{outer} \\ \text{Neumann} \\ \text{problem} \end{array} \quad \leftarrow \text{lines from inside}$$

$$\phi(x) = \int_{\partial V} \Lambda(x, x') B_n(x') ds'$$

Green's function  
for Neumann problem

Boundary condition for the »inner problem«

$$B_{\text{tang}}^{\omega} = -\nabla_{\text{tang } \partial V} \int_{\partial V} \Lambda(x, x') B_n(x') ds' \text{ on } \partial V$$

non-local condition!



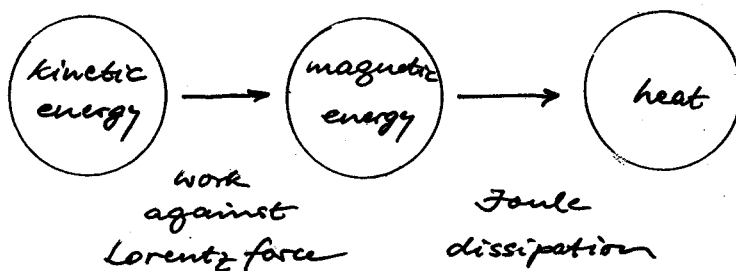
o 4.2.5.

Energy balance

$$\underbrace{\frac{d}{dt} \int_{\infty} \frac{B^2}{2\mu} dv}_{\text{total magnetic energy}} = - \underbrace{\int_V \frac{j^2}{\sigma} dv}_{\text{Joule heat production}} - \underbrace{\int_V u \cdot (j \times B) dv}_{\text{work done by } (j > 0) \text{ or against } (j < 0) \text{ Lorentz force}}$$

DYNAMO:

$$- \int_V u \cdot (j \times B) dv \geq \int_V \frac{j^2}{\sigma} dv \quad \left[ \begin{array}{l} R_m \geq R_{m \text{ crit}} \\ = O(1) \end{array} \right]$$



Dynamo requires stretching of magnetic field lines

o 4.2.6.

Time scales

$$T_\eta = \frac{L^2}{\eta} \quad \text{diffusive time scale}$$

$$T_U = \frac{L}{U} \quad \text{kinetic time scale}$$

$$\frac{T_\eta}{T_U} = R_m$$

$\lambda$  dynamo growth rate

$$\lambda T_U \rightarrow 0 \quad \text{as } R_m \rightarrow \infty$$

slow dynamo

$$\lambda T_U \rightarrow \text{positive value as } R_m \rightarrow \infty$$

fast dynamo

● 4.3.

(Anti-) Dynamo theorems

○ 4.3.1

Theorems concerning the intensity  
of the fluid motion

Lower bounds for (properly defined)  $R_m$

Backus 1958

Childress 1969

o 4.3.2.

Theorems concerning the geometry (symmetry) of the magnetic field

- Cowling's theorem Cowling 1934  
Braginsky 1964

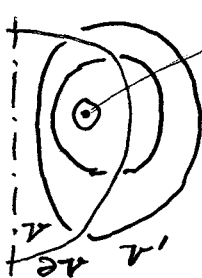
⋮

A magnetic field that is symmetric about any axis can never be maintained by a dynamo. //

- » Plane version « of this theorem

A magnetic field that is independent of one Cartesian coordinate (i.e., e.g.,  $B = B(x, y)$ ) can never be maintained by a dynamo.

- Cowling's neutral point argument for the steady case



neutral point inside the fluid

$$\nabla \times B = \mu_0 (E + u \times B)$$

$$\oint_{\partial \mathcal{V}} B \cdot dl = \int_{\mathcal{V}} \mu_0 (E + u \times B) \cdot ds$$

$\xrightarrow{\mathcal{V}}$        $\uparrow E_p = 0$   
 in meridional plane

$$\overline{B^2} L \leq \mu_0 |u|_{\max} \int_{\mathcal{V}} |B| \cdot ds$$

↑ assume  $> 0$

$$\approx = \mu_0 |u|_{\max} \overline{B} S$$

Consider limit  $L, S \rightarrow 0$

$$\underbrace{\overline{B^2} / \overline{B}}_{\rightarrow c > 0} \leq \mu_0 |u|_{\max} \underbrace{S/L}_{\rightarrow 0}$$

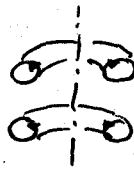
contradiction!

- Cowling's theorem breaks down if conductivity  $\sigma$  no longer isotropic Lortz 1989

o 4.3.3.

Theorems concerning the geometry  
of the fluid flow

• No analogue to Cowling's theorem!



• Gailitis 1970:

axisymmetric motion maintains  
a (non-axisymmetric) magnetic field

• Roberts 1972:

motion depending only on  $x$  and  $y$   
(but non-zero  $u_x, u_y$  and  $u_z$ )  
maintains a magnetic field  
(depending on  $x, y$  and  $z$ )

• Theorem by Bullard & Gellman

Bullard & Gellman 1954

Spherical body

$$\eta = \eta(r \text{ alone})$$

A magnetic field cannot be maintained  
by a purely toroidal motion  
(i.e.  $\nabla \cdot \mathbf{u} = 0$  and  $u_r = 0$ ).

• No dynamo by differential rotation alone!

• Theorem breaks down for non-radial  $\nabla \eta$

•  $\gg$  Plane version  $\ll$  of this theorem

Zeldovich 1956

$$\eta = \eta(z \text{ alone})$$

Zeldovich & Ružmaikin 1958

A magnetic field cannot be maintained  
by a motion in planes  $z = \text{const}$

(i.e.  $u_x = u_x(x, y, z, t), u_y = u_y(x, y, z, t), u_z = 0$ ).

• Theorem by Busse

Busse 1975

Which deviation from a toroidal motion  
is necessary for a dynamo?

Spherical body

$\eta = \text{const}$

Dynamo requires  $\frac{1/4 \omega r / \max}{\eta} \geq \frac{E^P}{E^P + E^T}$

$E^P, E^T$  energies stored in the poloidal  
and the toroidal parts  
of the magnetic field

o 4.3.4.

A presumption

In all spherical dynamo models investigated so far there is an interplay between the poloidal and the toroidal part of the magnetic field.

Presumption: no dynamo with purely poloidal or purely toroidal magnetic field.

A dynamo with a purely toroidal magnetic field would be an »invisible dynamo«, i.e., no magnetic field at the surface or outside the fluid body.

Arguments against invisible dynamos  
by Kaiser et al. 1974

● 4.4.

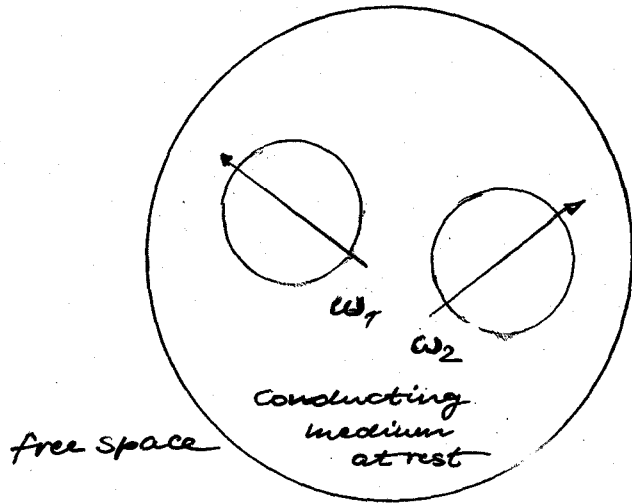
## *Developments of the idea of the dynamo*

○ 4.4.1.

- 1866 Werner von Siemens  
Charles Wheatstone  
*Principle of the self-exciting dynamo*
- 1919 Sir Joseph Larmor  
*Magnetic fields of the Sun (and the Earth) due to dynamo processes?*
- 1934 T. G. Cowling  
*Anti-dynamo theorem: No dynamo with axisymmetric magnetic field*
- 1954 E. Bullard and H. Gellman  
*Anti-dynamo theorem: No dynamo due to toroidal motion*
- 1955 E. N. Parker  
*The role of cyclonic convection in dynamo processes*
- 1958 E. Herzenberg  
*Existence proof for homogeneous dynamo*
- 1964 S. I. Braginsky  
*Theory of the nearly symmetric dynamo („ $\Gamma$ -effect“)*
- 1966 M. Steenbeck, F. Krause and K.-H. Rädler  
*Mean-field dynamo theory ( $\alpha$ -effect etc.)*
- 1968 D. Lortz
- 1973 Ju. B. Ponomarenko  
*Dynamos in infinite cylinders*
- 1972 G. O. Roberts  
*Spatially periodic dynamos*
- 1973 C. L. Pekeris, Y. Accad and B. Shkoller  
D. Gubbins
- 1974 S. Kumar and P. H. Roberts
- 1989 M. L. Dudley and R. W. James  
*Spherical kinematic dynamo models*
- ..... *Dynamo models for the Earth, the Sun,  
planets, stellar objects and galaxies  
Numerical simulations*
- 1999 *First successful runs of the Riga and Karlsruhe dynamo experiments*

○ 4.4.2.  
Herzenberg dynamo

Herzenberg 1958



Self-excitation of magnetic fields  
for special mutual positions of the rotation axes  
and sufficiently large angular velocities  $\omega_1$  and  $\omega_2$



● 4.5.

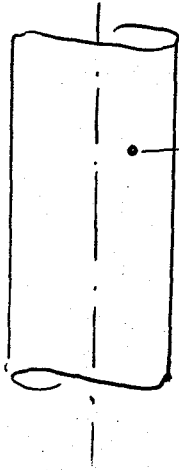
Examples of dynamos

working in an infinitely extended conducting medium

○ 4.5.1

Lortz dynamo

Lortz 1968



medium at rest  
• specific type  
of helical motion

Growing magnetic field  
(with helical structure)  
possible

A modification:

Lortz 1972

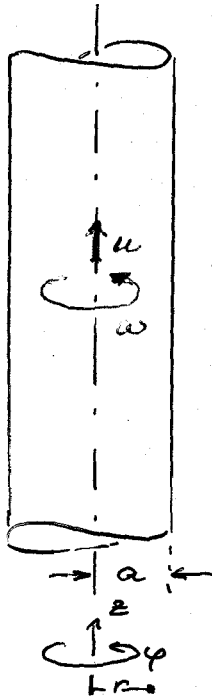
Cylinder → torus in free space

An example in which deviations  
of the magnetic from axisymmetry  
occur only in the fluid body,  
not in outer space

o 4.5.2.

Ponomarenko dynamo

Ponomarenko 1973



medium at rest

helical motion

$$B = \text{Re}(\hat{B}(r) \exp(i(m\varphi + kz) + pt))$$

$\hat{B}, p$  complex

$$R_{\omega} = \frac{\omega a^2}{\eta}, \quad R_u = \frac{u a}{\eta}$$

$$R_m = \sqrt{R_{\omega}^2 + R_u^2}$$

For rigid motion of the cylinder

$$\text{DYNAMO: } \underline{R_m \geq 17.722}$$

Marginal case:  $m = 1$

$$k/a = -0.3875$$

$$R_u/R_{\omega} = 1.3114$$

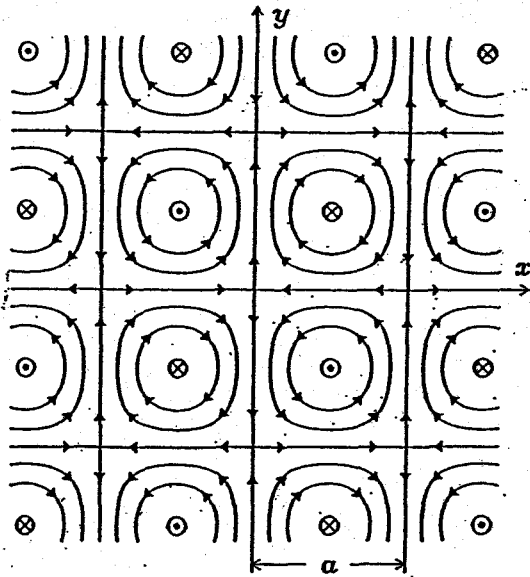
→ RIGA dynamo experiment

○ 4.5.3.

Roberts dynamo

G.O. Roberts 1972

(precursor:  
Gailitis 1967)



helicity  
 $u \cdot (\nabla \times u) \geq 0$

Example

$$u_x = -u_L \frac{\pi}{2} \sin\left(\frac{\pi x}{a}\right) \cos\left(\frac{\pi y}{a}\right)$$

$$u_y = u_L \frac{\pi}{2} \cos\left(\frac{\pi x}{a}\right) \sin\left(\frac{\pi y}{a}\right)$$

$$u_z = -u_H \left(\frac{\pi}{2}\right)^2 \sin\left(\frac{\pi x}{a}\right) \sin\left(\frac{\pi y}{a}\right)$$

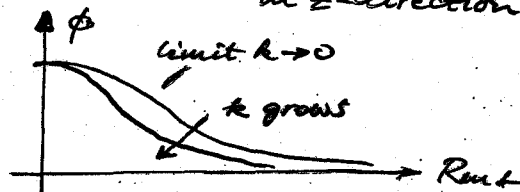
$$B = \text{Re}(\hat{B}(x, y) \exp(ikz + pt))$$

$$R_{mL} = \frac{u_L a}{2\eta} \quad R_{mH} = \frac{u_H a}{\eta}$$

$$\text{DYNAMO: } R_{mL} R_{mH} \phi(R_{mL}) \geq \frac{32}{\pi} \frac{a}{\ell}$$

$\ell = \frac{2\pi}{k}$  period length of  $B$   
in  $z$ -direction

These results  
can be  
obtained  
in a  
mean-field  
approach!



→ KARLSRUHE dynamo experiment

Roberts dynamo works also with a flow pattern  
modified such that  $u \cdot (\nabla \times u) = 0$

if  $a \cdot (\nabla \times a)$  predominantly  $> 0$   
or predominantly  $< 0$ ,  
where  $u = \nabla \times a$ ,  $\nabla \cdot a = 0$ .

● 4.6.

Dynamos in spherical fluid bodies

○ 4.6.1

Mathematical tools, Bullard-Gellman formalism

Consider

$$\left. \begin{aligned} \eta \nabla^2 B + \nabla \times F - \partial_t B &= 0 \\ \nabla \cdot B &= 0 \end{aligned} \right\} \text{in } r < R$$

$$\left. \begin{aligned} \nabla \times B &= 0 \\ \nabla \cdot B &= 0 \end{aligned} \right\} \text{in } r > R$$

Spherical coordinates  
 $r, \theta, \varphi$

For simplicity  $\eta = \text{const}$

$$[B] = 0 \text{ across } r = R$$

$$B \rightarrow 0 \text{ as } r \rightarrow \infty$$

Introduce  $B = B^P + B^T$  with  $\nabla \cdot B^P = 0$

$$\text{and } F = F^P + F^T \quad \ddagger \nabla \cdot F^P \text{ not necessarily } = 0$$

↪

$$\left. \begin{aligned} \eta \nabla^2 B^P + \nabla \times F^T - \partial_t B^P &= 0 \\ \eta \nabla^2 B^T + \nabla \times F^P - \partial_t B^T &= 0 \end{aligned} \right\} \text{in } r < R$$

$$\nabla \times B^P = 0, \quad B^T = 0 \text{ in } r > R$$

$$[B^P] = 0 \text{ across } r = R, \quad B^T = 0 \text{ on } r = R$$

$$B^P \rightarrow 0 \text{ as } r \rightarrow \infty$$

Introduce  $B^P = -\nabla \times (r \times \nabla S)$ ,  $B^T = -r \times \nabla T$ ,

$$\nabla \times F^P = +r \times \nabla F; \quad F^T = -r \times \nabla G$$

↪

$$\left. \begin{aligned} \eta \Delta S - G - \partial_t S &= 0 \\ \eta \Delta T - \Delta F - \partial_t T &= 0 \end{aligned} \right\} \text{in } r < R$$

$$\Delta S = 0, \quad T = 0 \text{ in } r > R$$

$$[S] = [\partial S / \partial r] = 0 \text{ across } r = R, \quad T = 0 \text{ on } r = R$$

$$S \rightarrow 0 \text{ as } r \rightarrow \infty$$

if  $S, T, F$  and  $G$  properly normalized

Expand  $S = \sum_{n,m} S_n^m(r,t) Y_n^m(\theta, \varphi)$   
spherical harmonics

$\leadsto$   $T, F, G$  analogously

$$\left. \begin{aligned} \eta D_n S_n^m - G_n^m - \partial_t S_n^m &= 0 \\ \eta D_n T_n^m - D_n^m F_n^m - \partial_t T_n^m &= 0 \end{aligned} \right\} \text{in } r < R \quad (*)$$
$$D_n f = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial f}{\partial r} \right) - \frac{n(n+1)}{r^2} f$$

$$(S_n^m \sim r^{-(n+1)}, T_n^m = 0 \text{ in } r > R)$$

$$\frac{\partial S_n^m}{\partial r} + \frac{n+1}{r} S_n^m = T_n^m = 0 \text{ at } r = R \quad (**)$$

Specify  $u$ , express  $u^P$  and  $u^T$  like  $B^P$  and  $B^T$   
by spherical harmonics,

calculate  $F_n^m$  and  $G_n^m$  as functions of  $S_{n'}^{m'}$ ,  $T_{n'}^{m'}$   
and their derivatives, e.g.,  $F_n^m = \sum_{n',m'} (FS)_{n'm'}^{m'} S_{n'}^{m'} + \dots$

Assume  $B \sim \exp(pt)$

$\leadsto S, T \sim \exp(pt)$

Equations (\*) together with boundary conditions (\*\*),

with  $F_n^m$  and  $G_n^m$  expressed by  $S_{n'}^{m'}$  and  $T_{n'}^{m'}$

and  $\partial_t$  replaced by  $p$ ,

pose an eigenvalue problem

with  $p$  as eigenvalue parameter.

o 4.6.2.

Special models

Bullard & Gellman 1954

no acceptable results,  
convergence problems

⋮

Pekeris, Accad & Shkoller 1973

Beltrami flows  $\nabla \times u = \lambda u$

Gubbins 1973

axisymmetric poloidal and toroidal  
flows

Kumar & Robert 1975

non-axisymmetric poloidal and toroidal  
flows

Dudley & James 1989

axisymmetric poloidal and toroidal  
flows

⋮

• 5.

## THE GENERAL DYNAMO PROBLEM

(DYNAMICALLY CONSISTENT DYNAMO MODELS)

• 5.1.

Thermally driven dynamos

For the sake of simplicity

Boussinesq-approximation

$\eta, \nu, \alpha, \tilde{\kappa}$  constants

$$\partial_t \mathbf{B} - \nabla \times (\mathbf{u} \times \mathbf{B}) = \eta \nabla^2 \mathbf{B}$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p + \nu \nabla^2 \mathbf{u} - 2\boldsymbol{\Omega} \times \mathbf{u}$$

$$\nabla \cdot \mathbf{u} = 0 \quad + \frac{1}{\rho} \mathbf{F} + \frac{1}{\rho \beta} (\nabla \times \mathbf{B}) \times \mathbf{B}$$

↑ buoyancy

Reference state  $\mathbf{B} = \mathbf{u} = 0$ ,  $\rho = \rho_0(\alpha)$ ,  $p = p_0(\alpha)$ ,  $T = T_0(\alpha)$

$$T = T_0 + \theta \quad \left\{ \begin{array}{l} \text{volume expansion} \\ \text{coefficient} \end{array} \right.$$

$$\mathbf{F} = \rho_0 \alpha \theta \mathbf{g} \leftarrow \text{gravitational acceleration}$$

$$\partial_t \theta + \mathbf{u} \cdot \nabla \theta = \kappa \Delta \theta - \mathbf{u} \cdot \nabla T_0$$

||  
 $\tilde{\kappa} / \rho c_v$

Choose values of

•  $P_m = \frac{\nu}{\eta}$  magnetic Prandtl number

•  $E = \frac{\nu}{\Omega L^2}$  Ekman number

$(Ta = (2/E)^2 = (\frac{2\Omega L^2}{\nu})^2$  Taylor number)

•  $P = \frac{\nu}{\kappa}$  Prandtl number

•  $Ra = \frac{\alpha g (\Delta T)_c L^4}{\kappa \nu}$  Rayleigh number

$(\Delta T)_c$  characteristic value of  $\Delta T_0$

Calculate solutions  $B, u, \theta$

$B, u$  characteristic values of  $B, u$

Solutions can be interpreted in terms of

•  $R_m = \frac{UL}{\eta}$  magnetic Reynolds number

•  $Re = \frac{UL}{\nu}$  Reynolds number

•  $Ro = \frac{U}{2\Omega L}$  Rossby number

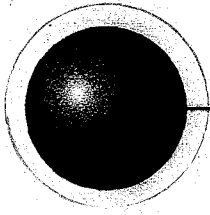
•  $N = \frac{\sigma B^2 L}{\rho u}$  Stuart number

•  $H = \frac{\sqrt{\sigma} BL}{\sqrt{\rho \nu}}$  Hartmann number

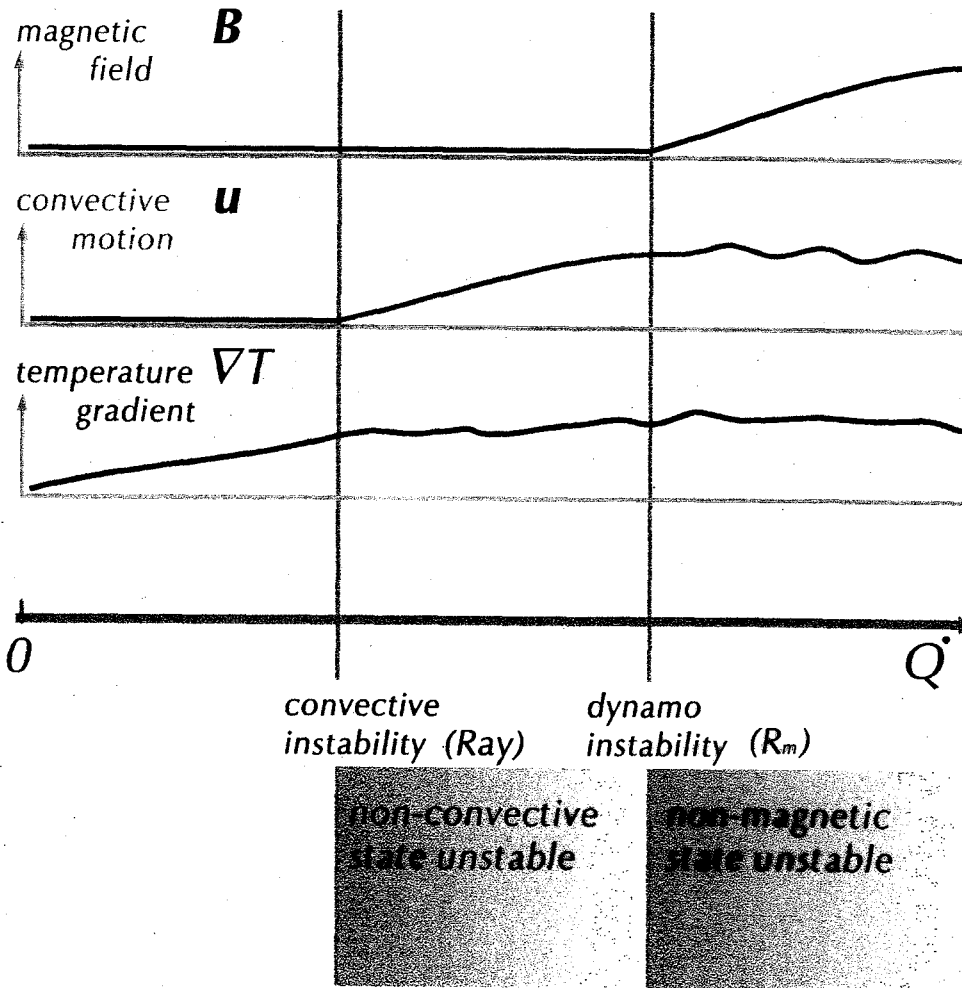
•  $\Lambda = \frac{\sigma B^2}{2\rho \Omega}$  Elsasser number

⋮





heat source  
 $\dot{Q}$



● 6.

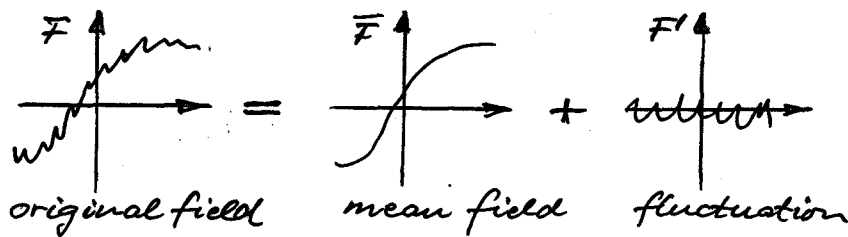
MEAN-FIELD ELECTRODYNAMICS

● 6.1.

The general concept

○ 6.1.1.

Mean fields and fluctuations



$F = \bar{F} + F'$        $\bar{F}$  defined by a proper averaging procedure

$\mathbf{F} = \bar{\mathbf{F}} + \mathbf{F}'$        $\mathbf{F} = e_i F_i$        $\bar{\mathbf{F}} = e_i \bar{F}_i$   
 unit vectors  
 w.r.t. Cartesian, spherical, cylindrical, ...  
 coordinate system

○ 6.1.2.

Reynolds rules

(R1)  $\overline{F+G} = \bar{F} + \bar{G}$

(R2)  $\overline{\bar{F}} = \bar{F} \quad \hookrightarrow \quad \overline{F'} = 0$

(R3)  $\overline{\bar{F}G} = \bar{F}\bar{G} \quad \hookrightarrow \quad \overline{\bar{F}G'} = \bar{F}\bar{G}, \quad \overline{\bar{F}G'} = 0$

(R4)  $\overline{\partial F / \partial x} = \partial \bar{F} / \partial x, \quad \overline{\partial F / \partial t} = \partial \bar{F} / \partial t$

$\overline{FG} = \bar{F}\bar{G} + \overline{F'G'}$

0 6.1.3.

### Examples of averages

□

Statistical (ensemble) average

$$\bar{F}(x,t) = \int F(x,t;p) f(p) dp$$

$$\int f(p) dp = 1$$

(R1)...(R4) apply exactly.

BUT: relation of averages to observable quantities?

□

Space averages

$$\bar{F}(x,t) = \int F(x;\xi,t) g(\xi) d^3\xi$$

$$\int g(\xi) d^3\xi = 1$$

(R2) and (R3) in general

violated,

apply approximately

in two-scale situations.

special case

» Braginsky's average «

$$\bar{F}(\dots, t) = \frac{1}{2\pi} \int_0^{2\pi} F(\dots, \varphi, t) d\varphi$$

(R1)...(R4) apply exactly.

BUT: mean fields by definition axisymmetric.

□

Time average

$$\bar{F}(x,t) = \int F(x, t+\tau) g(\tau) d\tau$$

$$\int g(\tau) d\tau = 1$$

(R2) and (R3) in general

violated,

apply approximately

in two-scale situations.

□

Averages by » filtering «

of spectra,

e.g.,

$$\bar{F}(x,t) = \int_{-\infty}^{\infty} \hat{F}(k,t) e^{ik \cdot x} d^3k$$

(R3) in general violated,

applies with special

(two-scale) assumptions

on the spectrum.

$$\bar{F}(x,t) = \int_{|k| \leq K} \hat{F}(k,t) e^{ik \cdot x} d^3k$$

• 6.2.

Basic equations for the mean electromagnetic fields

o 6.2.1.

Starting point

$$\begin{aligned} \nabla \times \mathbf{E} &= -\partial_t \mathbf{B} & \mathbf{B} &= \mu \mathbf{H} \\ \nabla \times \mathbf{H} &= \mathbf{j} & \mathbf{j} &= \sigma(\mathbf{E} + \mathbf{u} \times \mathbf{B}) \\ \nabla \cdot \mathbf{B} &= 0 \end{aligned}$$

$$\begin{aligned} \nabla \times (\eta \nabla \times \mathbf{B} - \mathbf{u} \times \mathbf{B}) + \partial_t \mathbf{B} &= 0 \\ \nabla \cdot \mathbf{B} &= 0 \end{aligned}$$

o 6.2.2.

Mean-field equations

Validity of the Reynolds rules assumed

$$\begin{aligned} \nabla \times \bar{\mathbf{E}} &= -\partial_t \bar{\mathbf{B}} & \bar{\mathbf{B}} &= \mu \bar{\mathbf{H}} \\ \nabla \times \bar{\mathbf{H}} &= \bar{\mathbf{j}} & \bar{\mathbf{j}} &= \sigma(\bar{\mathbf{E}} + \bar{\mathbf{u}} \times \bar{\mathbf{B}} + \underline{\underline{\mathbf{E}}}) \\ \nabla \cdot \bar{\mathbf{B}} &= 0 \end{aligned}$$

$$\begin{aligned} \nabla \times (\eta \nabla \times \bar{\mathbf{B}} - \bar{\mathbf{u}} \times \bar{\mathbf{B}} - \underline{\underline{\mathbf{E}}}) + \partial_t \bar{\mathbf{B}} &= 0 \\ \nabla \cdot \bar{\mathbf{B}} &= 0 \end{aligned}$$

$\mathbf{E} = \overline{\mathbf{u}' \times \mathbf{B}'}$  mean electromotive force due to fluctuations of the motion and the magnetic field

0 6.2.3.

Properties of the mean electromotive force

$$\mathbf{E} = \overline{u' \times B'}$$

$$\nabla \times (\eta \nabla \times B' - \bar{u} \times B' - \overline{u' \times B'} - \overline{u' \times B'}) + \partial_t B' = \nabla \times (u' \times \bar{B})$$

$$\nabla \cdot B' = 0 \quad - (u' \times B')'$$

$$B' = B^{(0)} + B^{(B)}$$

$$E = E^{(0)} + E^{(B)}$$

functional of  $\bar{u}$ ,  $u'$  and  $\bar{B}$ ,  
linear and homogeneous in  $\bar{B}$   
functional of  $\bar{u}$  and  $u'$

$E$  depends only via averaged quantities on  $u'$ .

Assume until further notice

← see 6.6.

that  $B'$  decays to zero if  $\bar{B} = 0$

(i.e. no small-scale dynamics,

purely hydrodynamic  $\Rightarrow$  background turbulence  $\leftarrow$ ).

$\leadsto$

$E^{(0)}$  decays to zero

$$\underline{E_i(x,t)} = \int \int_{-\infty}^{\infty} K_{ij}(x,t;\xi,\tau) \bar{B}_j(x-\xi, t-\tau) d^3\xi d\tau \quad (*)$$

depends on  $\bar{u}$  and  $u'$  only,  
vanishes for large  $|\xi|$  and  $\tau$

Assume  $\gg$  nearly local and instantaneous  $\ll$   
dependence of  $\bar{E}$  on  $\bar{B}$

$$\bar{E}_i = a_{ij} \bar{B}_j + b_{ijk} \partial \bar{B}_j / \partial x_k + \dots \quad \uparrow \quad (**)$$

$a_{ij}$  and  $b_{ijk}$ 
depend on  $\bar{u}$  and  $\bar{u}'$  only

$$a_{ij} = \int_0^\infty \int_0^\infty K_{ij}(x, t; \xi, \tau) d^3\xi d\tau \quad (***)$$

$$b_{ijk} = - \int_0^\infty \int_0^\infty K_{ij}(x, t; \xi, \tau) \xi_k d^3\xi d\tau$$

Relations (\*\*), (\*\*\*) and (\*\*\*) apply  
in the case of a (given) dependence  
of  $\bar{u}$  and  $\bar{u}'$  on  $\bar{B}$ , too.

However, this case is discussed only later.

See 6.7.

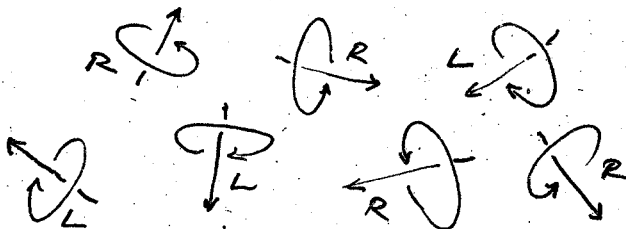
• 6.2.

## Definitions concerning turbulence

### Turbulence

- homogeneous  
if all mean quantities depending on  $u'$   
are invariant under translation of  $u'$
- steady  
... under time shift in  $u'$
- axisymmetric  
... under rotation of  $u'$  about a given axis
- isotropic  
... under rotation of  $u'$  about arbitrary axes
- reflectionally symmetric  
(mirror-symmetric)  
w.r.t. a given plane or a given point  
... under reflexion of  $u'$  about this plane  
or at this point
- reflectionally symmetric  
(mirror-symmetric, gyrotropic)  
... under reflexion of  $u'$  about arbitrary planes  
or at arbitrary points

Under reflexion right-handed structures  
turn into left-handed ones  
and vice versa.



● 6.4.

A simple (academic) example:

$$\bar{u} = 0$$

$u'$  homogeneous isotropic turbulence

$\eta$  constant

○ 6.4.1.

The structure of  $\bar{E}$

$$E_i = a_{ij} \bar{B}_j + b_{ijk} \partial \bar{B}_j / \partial x_k$$

$u'$  homogeneous turbulence

$\leadsto a_{ij}, b_{ijk}$  independent of position

$u'$  isotropic turbulence

$\leadsto a_{ij}, b_{ijk}$  isotropic tensors

(i.e., their components do not change under rotations of the coordinate system about arbitrary axes)

$$a_{ij} = \alpha \delta_{ij}, \quad b_{ijk} = \beta \epsilon_{ijk}$$

$\underbrace{\hspace{10em}}_{\text{determined by } u'}$

$$\bar{E} = \alpha \bar{B} - \beta \underbrace{\nabla \times \bar{B}}_{\mu \bar{J}}$$

○ 6.4.2.

Ohm's law for mean fields

$$\bar{J} = \sigma (\bar{E} + \bar{E})$$

$$\bar{J} = \frac{\sigma}{1 + \mu \sigma \beta} (\bar{E} + \alpha \bar{B})$$

$\sigma_M \leftarrow$  mean-field conductivity  $\ll \alpha$ -effect $\ll$



0 6.4.3.

The dependence of  $\alpha$  and  $\beta$

on symmetry properties of  $u'$

$$\text{Relation } \bar{E} = \overline{u' \times B'} = \alpha \bar{B} - \beta \nabla \times \bar{B} \quad (\#)$$

has to be considered as a consequence

$$\text{of } \nabla \times (\eta \nabla \times B - u \times B) + \partial_t B = 0, \quad \nabla \cdot B = 0, \quad (\#\#)$$

with  $B = \bar{B} + B'$  and  $u = u'$ .

Equations ( $\#\#$ ) remain valid if  $\bar{B}$ ,  $B'$  and  $u'$

are reflected at  $x=0$ ,

i.e., replaced by  $\bar{B}'^{rk}$ ,  $B''^{rk}$  and  $u''^{rk}$ ,

$$\text{where } F''^{rk}(x) = -F(-x).$$

The same has to apply to ( $\#$ ).

Original relation ( $\#$ ) at  $x=0$ :

$$\overline{u'(0) \times B'(0)} = \alpha(u') \bar{B}(0) - \beta(u') (\nabla \times \bar{B})(0) \quad (X)$$

Modified relation ( $\#$ ) at  $x=0$ :

$$\overline{u''^{rk}(0) \times B''^{rk}(0)} = \alpha(u''^{rk}) \bar{B}'^{rk}(0) - \beta(u''^{rk}) (\nabla \times \bar{B}'^{rk})(0)$$

$$\overline{u'(0) \times B'(0)} = -\alpha(u''^{rk}) \bar{B}(0) - \beta(u''^{rk}) (\nabla \times \bar{B})(0) \quad (XX)$$

$$\left\{ \begin{aligned} (\nabla \times \bar{B})_x &= \frac{\partial \bar{B}_z(\vec{x})}{\partial y} - \frac{\partial \bar{B}_y(\vec{x})}{\partial z} \\ (\nabla \times \bar{B}'^{rk})_x &= \frac{\partial \bar{B}_z(-\vec{x})}{\partial(-y)} - \frac{\partial \bar{B}_y(-\vec{x})}{\partial(-z)} \\ \Rightarrow (\nabla \times \bar{B}'^{rk})(0) &= (\nabla \times \bar{B})(0) \end{aligned} \right.$$

Comparison of (X) and (XX)

$$\Rightarrow \underline{\alpha(u''^{rk}) = -\alpha(u')}, \quad \underline{\beta(u''^{rk}) = \beta(u')} \quad \parallel$$

If turbulence reflectionally symmetric

then  $\alpha = 0$

o 6.4.4.

Dynamo action of a homogeneous isotropic  
not reflectionally symmetric turbulence

$$\eta_M \nabla^2 \bar{B} + \alpha \nabla \times \bar{B} - \frac{\partial \bar{B}}{\partial t} = 0 \quad \eta_M = \eta + \beta$$

$$\nabla \cdot \bar{B} = 0 \quad (\text{suppose } > 0)$$

Ansatz

$$\bar{B} = \text{Re}(\hat{B} \exp\{i k x + p t\})$$

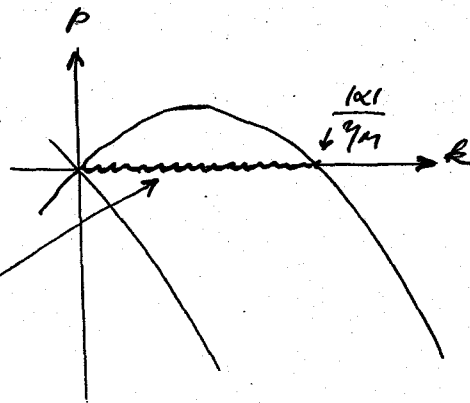
$$\begin{aligned} \leadsto \\ (\eta_M k^2 + p) \hat{B} - \alpha i k \times \hat{B} &= 0 \\ k \cdot \hat{B} &= 0 \end{aligned}$$

Specify coordinate system so that  $k = (0, 0, k)$

$$\begin{aligned} \leadsto \\ (\eta_M k^2 + p) \hat{B}_x + i \alpha k \hat{B}_y &= 0 \\ i \alpha k \hat{B}_x - (\eta_M k^2 + p) \hat{B}_y &= 0 \\ \hat{B}_z &= 0 \end{aligned}$$

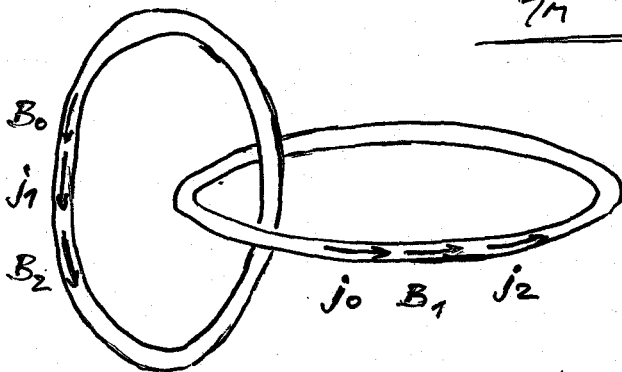
$$\leadsto (\eta_M k^2 + p)^2 = \alpha^2 k^2$$

$$\leadsto p = -\eta_M k^2 \pm i \alpha k$$



$$\text{DYNAMO: } k \leq \frac{|\alpha|}{\eta_M}$$

$$k = \frac{2\pi}{\ell}: \quad \frac{|\alpha| \ell}{\eta_M} \geq 2\pi$$



$$\nabla \times B = \mu j$$

$$j = \sigma(E + \alpha B)$$

$$\alpha > 0$$

0 6.4.5.

The coefficients  $\alpha$  and  $\beta$  as functions of  $u'$

$$\eta \nabla^2 B' - \partial_t B' = -\nabla \cdot (u' \times B + \underbrace{u' \times B' - u' \times B}) , \nabla \cdot B' = 0$$

First-order smoothing approximation (FOSA)

= Second-order correlation approximation (SOCA):

assume  $u'$  is so small that  $|B'| \ll |B|$   
and cancel  $\bigcirc$ .

Remember heat conduction equation

$$\eta \Delta T - \partial_t T = -q$$

$$T(x,t) = \int_{-\infty}^t \int_{-\infty}^{\infty} G(x-x', t-t') q(x', t') d^3x' dt'$$

$$G(x,t) = (4\pi\eta t)^{-3/2} \exp(-x^2/4\eta t)$$

$$\eta \Delta G - \partial_t G = 0 \text{ for } t > 0$$

$$G(x,t) \rightarrow \delta^3(x) \text{ as } t \rightarrow +0$$

$$B'_k(x,t) = \int_{-\infty}^t \int_{-\infty}^{\infty} G(x-x', t-t') B'_k(x', t') d^3x' dt'$$

$$+ \varepsilon_{k\ell m} \varepsilon_{mnp} \int_{-\infty}^t \int_{-\infty}^{\infty} G(x-x', t-t') \frac{\partial}{\partial x'_\ell} (u'_n(x', t') \bar{B}_p(x', t')) d^3x' dt' \quad (*)$$

$$E_i(x,t) = \varepsilon_{ijk} u'_j(x,t) B'_k(x,t)$$

$$= \int_{-\infty}^t \int_{-\infty}^{\infty} K_{ip}(x,t;\xi,\tau) \bar{B}_p(x-\xi, t-\tau) d^3\xi d\tau$$

Substitute

$x' = x - \xi, t' = t - \tau$  in (\*) and let  $t_0 \rightarrow -\infty$

$$K_{ip}(x,t;\xi,\tau) = \varepsilon_{ijk} \varepsilon_{k\ell m} \varepsilon_{mnp}$$

$$\frac{1}{\xi} \frac{\partial G(\xi,\tau)}{\partial \xi_\ell} u'_j(x,t) u'_n(x+\xi, t-\tau) \delta_{\ell p} + \frac{\partial v_i(x,t;\xi,\tau)}{\partial \xi_p}$$

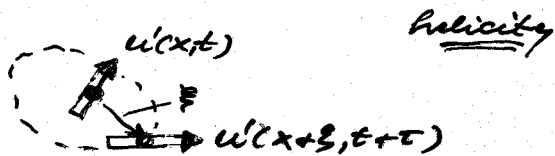
no  
x-dependence  
in this example

$v_i$  arbitrary vector field

$$\alpha = \frac{1}{3} a_{ii}$$

$$= -\frac{1}{3} \int_0^\infty \int \int Q(\xi, \tau) \overline{u(x, t) \cdot (\nabla \times u(x + \xi, t - \tau))} d^3 \xi d\tau$$

$$\overline{u(x, t) \cdot (\nabla \times u(x + \xi, t + \tau))} = h(\xi, \tau)$$



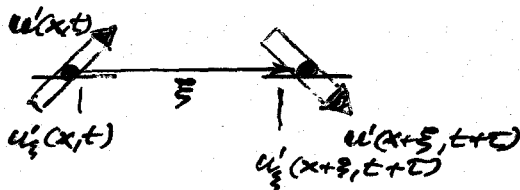
$$\beta = \frac{1}{6} \epsilon_{ijk} b_{ijk}$$

$$u'_i = (a_i \cdot \xi) / \xi$$

$$= - \int_0^\infty \int \int \frac{\partial Q(\xi, \tau)}{\partial \xi} \overline{u'_i(x, t) u'_i(x + \xi, t - \tau)} \xi d^3 \xi d\tau$$

$$\overline{u'_i(x, t) u'_i(x + \xi, t + \tau)} = l(\xi, \tau)$$

longitudinal correlation function



- High-conductivity limit  $\eta \rightarrow 0$ ,  $\left\{ \begin{array}{l} G(\mathbf{x}, \tau) \rightarrow \delta^3(\mathbf{x}) \\ \text{if } \eta \rightarrow 0 \end{array} \right.$   
more precisely  $\eta \tau_{\text{cor}} / \lambda_{\text{cor}}^2 \rightarrow 0$

$$\alpha = -\frac{1}{3} \overline{\int_0^{\infty} \mathbf{u}'(\mathbf{x}, t) \cdot (\nabla \times \mathbf{u}'(\mathbf{x}, t-\tau)) dt}$$

$$= -\frac{1}{3} \overline{\mathbf{u}' \cdot (\nabla \times \mathbf{u}')} \tau_{\text{cor}} \quad \parallel \quad \begin{array}{l} \text{different signs} \\ \text{of } \alpha \text{ and helicity} \end{array}$$

$$\beta = \frac{1}{3} \overline{\int_0^{\infty} (\mathbf{u}'(\mathbf{x}, t) \cdot \mathbf{u}'(\mathbf{x}, t-\tau)) dt}$$

$$= \frac{1}{3} \overline{u'^2} \tau_{\text{cor}} \quad \parallel$$

Sufficient (but not necessary) for validity:

$$u' \tau_{\text{cor}} / \lambda_{\text{cor}} \ll 1$$

Solar convection zone

$$\sigma = 3 \cdot 10^3 \text{ S/m}$$

$$u' = 2 \cdot 10^2 \text{ m/s}$$

$$\tau_{\text{cor}} = 3 \cdot 10^2 \text{ s}$$

$$\lambda_{\text{cor}} = 2 \cdot 10^6 \text{ m}$$

granules

$\Rightarrow$

$$\eta \tau_{\text{cor}} / \lambda_{\text{cor}}^2 = 2 \cdot 10^{-5}$$

$$u' \tau_{\text{cor}} / \lambda_{\text{cor}} = 3 \cdot 10^{-2}$$

$$\frac{\sigma_M}{\sigma} = (1 + \mu_0 \beta)^{-1}$$

$$= 0.7 \cdot 10^{-4}$$

- Low-conductivity limit  $\eta \rightarrow \infty$ ,  
more precisely  $\eta \tau_{\text{cor}} / \lambda_{\text{cor}}^2 \rightarrow \infty$   $\left\{ \begin{array}{l} \int_0^{\infty} G(\xi, t) dt \\ = \frac{1}{4\pi\eta\tau} \end{array} \right.$

$$\alpha = -\frac{1}{12\pi\eta\infty} \int \overline{u'_i(x,t) \cdot (\nabla \times u'_i(x+\xi, t))} \xi^{-1} d^3\xi$$

$$\beta = \frac{1}{12\pi\eta\infty} \int \overline{u'_i(x,t) u'_i(x+\xi, t)} \xi^{-1} d^3\xi$$

For an alternative representation  
put  $u' = \nabla \times a' + \nabla \varphi'$ ,  $\nabla \cdot a' = 0$ .

$$\left\{ \begin{array}{l} a'(x) = \frac{1}{4\pi} \int (\nabla \times u'(x+\xi)) \xi^{-1} d^3\xi \end{array} \right.$$

$$\alpha = -\frac{1}{3\eta} \overline{a' \cdot (\nabla \times a')}$$

$$\beta = \frac{1}{3\eta} (\overline{a'^2} - \overline{\varphi'^2})$$

$$\text{If } \overline{u'_i(x,t) u'_i(x+\xi, t)} = \frac{1}{3} \overline{u'^2} \exp(-\xi^2 / 2\lambda_{\text{cor}}^2)$$

$$\text{then } \beta = \frac{1}{9} \frac{\overline{u'^2} \lambda_{\text{cor}}^2}{\eta}$$

$$\frac{\beta}{\eta} = \frac{1}{9} R_{\text{M}}^2, \quad R_{\text{M}} = \frac{u' \lambda_{\text{cor}}}{\eta}$$

Sufficient (but not necessary) for validity:

$$R_{\text{M}} = \frac{u' \lambda_{\text{cor}}}{\eta} \ll 1$$

● 6.5.

More realistic cases

(i.e.  $\bar{u}$  no longer necessarily = 0,

$u'$  no longer homogeneous isotropic turbulence)

○ 6.5.1.

A simple (but realistic) example

$$\bar{u} = 0$$

$u'$  axisymmetric turbulence

preferred axis defined by a vector  $\lambda$

$a_{ij}, b_{ijk}$  axisymmetric tensors

$$a_{ij} = a_1 \delta_{ij} + a_2 \varepsilon_{ij\ell} \ell_\ell + a_3 \lambda_i \lambda_j$$

$$b_{ijk} = b_1 \varepsilon_{ijk} \quad \text{because } \partial \bar{E}_j / \partial x_j = 0$$

$$+ b_2 \delta_{ij} \lambda_k + b_3 \delta_{ik} \lambda_j + b_4 \delta_{jk} \lambda_i \quad \text{without interest!}$$

$$+ b_5 \varepsilon_{ij\ell} \ell_\ell \lambda_k + b_6 \varepsilon_{ik\ell} \ell_\ell \lambda_j + b_7 \varepsilon_{j\ell k} \ell_\ell \lambda_i$$

$$+ b_8 \lambda_i \lambda_j \lambda_k \quad \text{without loss of generality } b_6 = b_5,$$

$$\text{for } \varepsilon_{ij\ell} \ell_\ell \lambda_k - \varepsilon_{ik\ell} \ell_\ell \lambda_j$$

$$= \varepsilon_{ijk} \lambda^2 - \varepsilon_{j\ell k} \ell_\ell \lambda_i$$

$$\bar{E} = a_1 \bar{B} - a_2 \lambda \times \bar{B} + a_3 (\lambda \cdot \bar{B}) \lambda$$

Coefficients  $a_1, a_2, \dots, b_8$

$$- b_1 \nabla \times \bar{B}$$

may depend on  $|\lambda|$

$$+ b_2 \lambda \cdot \nabla \bar{B} + b_3 \lambda \cdot \nabla \bar{B}$$

$$- b_5 \lambda \times (\lambda \cdot \nabla \bar{B} + \lambda \cdot \nabla \bar{B}) - b_7 (\lambda \cdot (\nabla \times \bar{B})) \lambda$$

$$+ b_8 (\lambda \cdot (\lambda \cdot \nabla \bar{B})) \lambda$$

$$(\lambda \cdot \nabla \bar{B})_i = \lambda_j \frac{\partial \bar{B}_i}{\partial x_j} = (\lambda \cdot \nabla \bar{B})_i$$

$$(\lambda \cdot \nabla \bar{B})_i = \lambda_j \frac{\partial \bar{B}_j}{\partial x_i} = (\nabla (\lambda \cdot \bar{B}))_i$$

if  $\lambda$  constant

- Assume that  $u'$  reflectionally symmetric about planes containing  $\lambda$   
 $\lambda = g$  (e.g., gradient of turbulence intensity)

$$a_1 = a_3 = b_2 = b_3 = b_8 = 0$$

$$\begin{aligned} \mathcal{E} = & -a_2 g \times \bar{B} \quad \leftarrow \text{transport of mean magnetic flux} \\ & -b_1 \nabla \times \bar{B} \quad \gg \text{turbulent diamagnetism} \ll \\ & \text{- terms of 2nd order in } g \quad \gg \text{pumping of ... flux} \ll \end{aligned}$$

Rädler 1966

- Assume that  $u'$  reflectionally symmetric about plane perpendicular to  $\lambda = \Omega$  (e.g., Coriolis force)

$$a_1 = a_2 = a_3 = 0$$

$$\mathcal{E} = -b_1 \nabla \times \bar{B}$$

$$\begin{aligned} & \frac{+b_2 \Omega \nabla \bar{B} + b_3 \Omega \cdot \nabla \bar{B}}{\text{+ terms of 2nd and 3rd order in } \Omega} * \quad \begin{aligned} & \Omega \times (\nabla \times \bar{B}) \\ & = -(\Omega \cdot \nabla) \bar{B} \\ & + \nabla(\Omega \cdot \bar{B}) \end{aligned} \end{aligned}$$

$$* = -b_2 \Omega \times (\nabla \times \bar{B}) - (b_2 - b_3) \nabla(\Omega \cdot \bar{B})$$

↑  $\gg \Omega \times \bar{B}$ -effect  $\ll$

in combination with differential rotation capable of dynamo action

See 2.3.4.

- No  $\alpha$ -effect as soon as  $u'$  reflectionally symmetric about any plane!!!





0 6.5.4.

Symmetry properties of the basic equations  
and consequences for the structure of  $\mathcal{E}$

$$\left. \begin{aligned} \nabla \times \mathbf{E} &= -\partial_t \mathbf{B} & \mathbf{B} &= \mu \mathbf{H} \\ \nabla \cdot \mathbf{B} &= 0 & \mathbf{j} &= \sigma(\mathbf{E} + \mathbf{u} \times \mathbf{B}) \\ \nabla \times \mathbf{H} &= \mathbf{j} \end{aligned} \right\} (*)$$

If these equations are satisfied with  $\mathbf{B}, \mathbf{H}, \mathbf{E}, \mathbf{j}$  and  $\mathbf{u}$   
they are, too,

- if  $\mathbf{B}, \mathbf{H}, \mathbf{E}, \mathbf{j}$  and  $\mathbf{u}$  are subject to a rotation  
about an arbitrary axis (ROT)
- if  $\mathbf{B}, \mathbf{H}, \mathbf{E}, \mathbf{j}$  and  $\mathbf{u}$  are subject to a reflexion  
about an arbitrary plane or at any point (RFL)  
and, in addition,  $\mathbf{B}$  and  $\mathbf{H}$  to an inversion  
of their signs (SGN)

Define an operation  $\text{RFL}^*$  which acts  
like RFL on  $\mathbf{E}, \mathbf{j}$  and  $\mathbf{u}$   
and like RFL plus SGN on  $\mathbf{B}$  and  $\mathbf{H}$ .

If the above equations are satisfied  
with  $\mathbf{B}, \mathbf{H}, \mathbf{E}, \mathbf{j}$  and  $\mathbf{u}$   
they are, too, if these fields are subject  
to the operations ROT or  $\text{RFL}^*$ .

Define in addition to the »true« scalars, vectors and tensors, which behave under both rotations and reflexions of the (Cartesian) coordinate system like

$$S' = S, \quad V_i' = a_{ik} V_k, \quad T_{ij}' = a_{ik} a_{je} T_{ke}, \dots$$

»pseudo« scalars, vectors and tensors behaving under rotations in the same way but under reflexions like  $S' = -S, \quad V_i' = -a_{ik} V_k, \quad T_{ij}' = -a_{ik} a_{je} T_{ke}, \dots$ .

$\left. \begin{array}{l} \text{true vector} = \text{polar vector} \\ \text{pseudo vector} = \text{axial vector} \end{array} \right\}$

- $\delta_{ij}$ , defined such that always  $\delta_{11} = 1$ , is a true tensor
- $\epsilon_{ijk}, \dots \quad \dots \quad \epsilon_{123} = 1$ , is a pseudo tensor
- $(V \cdot W)$ , with both  $V$  and  $W$  being either true or pseudo vectors, is a true scalar
- $(V \cdot W)$ , with  $V$  being a true and  $W$  pseudo vector, is a pseudo scalar
- $V \times W, \dots$  both  $V$  and  $W \dots$  either true or pseudo vector, is a pseudo vector
- $V \times W, \dots V \dots$  true  $\dots W \dots$  pseudo vector, is a true vector
- $\nabla \times V$ , with  $V$  being a true vector, is a pseudo vector
- $\nabla \times V, \dots V \dots$  pseudo vector, is a true vector

System (\*)

with  $E, j$  and  $u$  understood as true

and  $B$  and  $H$  as pseudo quantities

contains only equalities

between either true or pseudo quantities

(i.e. not between a true and a pseudo quantity).

The same must apply for all consequences of (\*),

e.g.,

$$\underline{\underline{E}}_i = \underline{\underline{a}}_{ij} \underline{\underline{B}}_j + \underline{\underline{b}}_{ijk} \partial \underline{\underline{B}}_j / \partial x_k \quad - \text{true}$$

or

$$\underline{\underline{E}} = -\underline{\underline{\alpha}} \cdot \underline{\underline{B}} - \underline{\underline{j}} \times \underline{\underline{B}} \quad = \text{pseudo}$$

$$-\underline{\underline{\beta}} \cdot \nabla \times \underline{\underline{B}} - \underline{\underline{\delta}} \times (\nabla \times \underline{\underline{B}}) - \underline{\underline{\kappa}} \cdot (\nabla \underline{\underline{B}})^{(2)}$$

Extension of the concept to other basic equations,

e.g.,

$$\underline{\underline{\rho}} (\underline{\underline{\partial}}_t \underline{\underline{u}} + (\underline{\underline{u}} \cdot \nabla) \underline{\underline{u}}) = -\underline{\underline{\nabla}} p + \underline{\underline{\rho}} f - 2\underline{\underline{\rho}} \underline{\underline{\nabla}} \times \underline{\underline{u}}$$

o 6.5.5.

### Inhomogeneous turbulence

influenced by the Coriolis force and a mean motion

- Consider  $\mathcal{E}$  at a given point  $x = x_0$  in a rotating frame of reference. Note that  $\mathcal{E}$ , considered as a vector, is the same in other frames, too.
- Specify the frame so that  $\bar{u} = 0$  at  $x = x_0$ , denote the angular velocity responsible for the Coriolis force by  $\Omega$  and the (tensorial) gradient of  $\bar{u}$  by  $\nabla\bar{u}$ .
- Assume that the inhomogeneity of the turbulence can be described by a vector  $g$ .
- Assume that any helicity of the turbulence occurs only as a consequence of  $\Omega$ ,  $\nabla\bar{u}$  and  $g$ .
- Assume that in the relevant surroundings of the point  $x = x_0$  both  $\nabla\bar{u}$  and  $g$  can be considered as constant.

### Construction elements for $\mathcal{E}$

- isotropic tensors  $\delta_{ij}$  and  $\epsilon_{ijk}$   
Higher-rank isotropic tensors are combinations of them
- $\Omega$ ,  $\nabla\bar{u}$  and  $g$

$$(\nabla\bar{u})_{ij} = (\nabla\bar{u})_{ij}^{(s)} - \frac{1}{2}\epsilon_{ijk}\omega_k, \quad \omega = \nabla \times \bar{u}$$

No pseudo scalars independent of  $\Omega$ ,  $\nabla\bar{u}$  and  $g$ !

- Assume (for simplicity only) that the effects of  $\Omega$ ,  $\nabla\bar{u}$  and  $g$  are weak enough so that  $\mathcal{E}$  can be considered as
  - linear in  $\Omega$  and  $\nabla\bar{u}$  no rapid rotation!
  - linear in  $g$  ← Contributions to  $\mathcal{E}$  bilinear
 and that  $\nabla \cdot \bar{u} = 0$ . in  $\Omega$  and  $g$  or  $\nabla\bar{u}$  and  $g$  admitted!

$$\mathcal{E} = -\alpha \cdot \bar{B} - \gamma \kappa \bar{B} - \beta \cdot \nabla \times \bar{B} - \delta \times (\nabla \times \bar{B}) - \kappa \cdot (\nabla \bar{B})^{(S)}$$

$$\alpha_{ij} = \alpha_1^{(R)} (g \cdot \Omega) \delta_{ij} + \alpha_2^{(R)} (g_i \Omega_j + g_j \Omega_i) \quad C1$$

$$+ \alpha_1^{(W)} (g \cdot \omega) \delta_{ij} + \alpha_2^{(W)} (g_i \omega_j + g_j \omega_i) \quad C2$$

$$+ \alpha^{(us)} (\varepsilon_{iem} (\nabla \bar{u})_{ej}^{(S)} + \varepsilon_{jem} (\nabla \bar{u})_{ei}^{(S)}) g_m$$

$$\gamma_i = \gamma^{(0)} g_i$$

$$+ \gamma^{(R)} \varepsilon_{iem} g_e \Omega_m + \gamma^{(W)} \varepsilon_{iem} g_e \omega_m$$

$$+ \gamma^{(us)} (\nabla \bar{u})_{ie}^{(S)} g_e$$

$$\beta_{ij} = \beta^{(0)} \delta_{ij}$$

$$+ \beta^{(us)} (\nabla \bar{u})_{ij}^{(S)}$$

$$\alpha_1^{(R)}, \alpha_2^{(R)}, \dots, \kappa^{(us)}$$

functions of C3  
turbulence intensity,  
density stratification etc.

$$\delta_i = \delta^{(R)} \Omega_i + \delta^{(W)} \omega_i \quad C4$$

$$\kappa_{ijk} = \kappa^{(R)} (\delta_{ij} \Omega_k + \delta_{ik} \Omega_j) + \kappa^{(W)} (\delta_{ij} \omega_k + \delta_{ik} \omega_j)$$

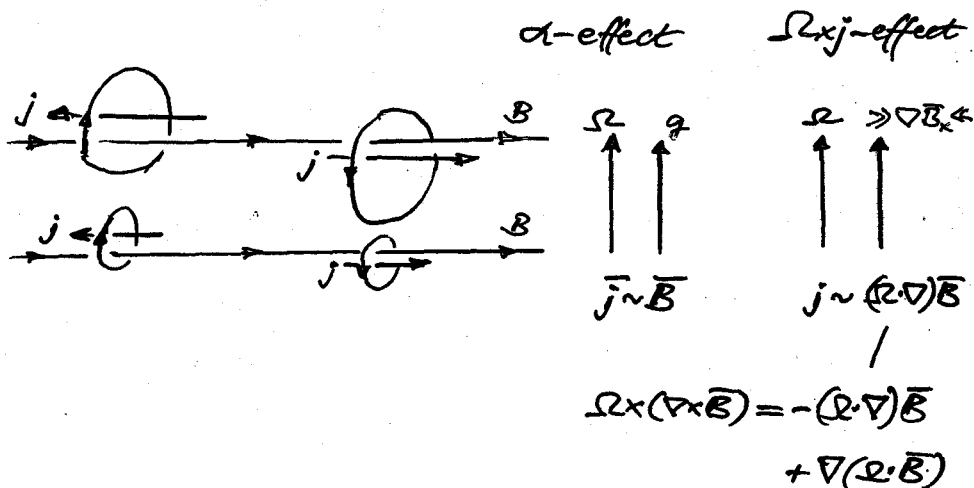
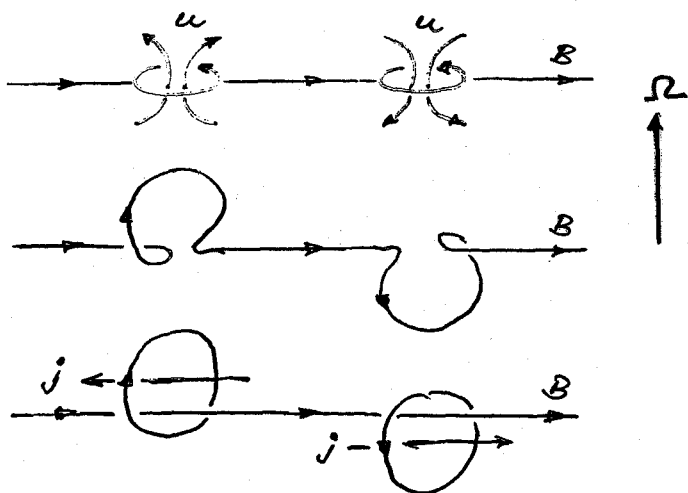
$$+ \kappa^{(us)} (\varepsilon_{ije} (\nabla \bar{u})_{ek}^{(S)} + \varepsilon_{ike} (\nabla \bar{u})_{ej}^{(S)})$$

Rädler, Kleorin & Rogachevskii 2003

Rogachevskii & Kleorin 2003

C1 & C4

Magnetic field lines and convective motions



Under realistic conditions an  $\alpha$ -effect occurs only as a consequence of both

- an inhomogeneity of the turbulence
- and the influence of a Coriolis force ( $-\Omega$ ) or of a mean motion ( $\langle w, (\nabla \bar{u})^{(s)} \rangle$ ).

The  $\beta$ -effect (which in combination with differential rotation is also capable of dynamo action) works already with an homogeneous turbulence under the influence of a Coriolis force ( $\Omega$ ) or of a mean motion ( $\langle w \rangle$ ).

## C2 & C3

If the assumption of weak influence  
of the Coriolis force is relaxed  
(i.e. rapid rotation is admitted)

new terms occur in  $\alpha_{ij}$  and  $\beta_{ij}$ ,  
e.g.,

$$\alpha_{ij} = \dots + \alpha_3^{(R)} (g \cdot \Omega) \Omega_i \Omega_j$$

$$\beta_{ij} = \dots + \beta_1^{(R)} \Omega_i \Omega_j,$$

and all coefficients may depend on  $|\Omega|$ .



● 6.6.

The case of MHD turbulence

○ 6.6.1

Extension of the concept discussed so far

Assume now

that  $B'$  does not decay to zero if  $\bar{B} = 0$

(i.e., existence of a small-scale dynamo,  
 » background turbulence « no longer purely hydrodynamic).

Denote  $u'$  and  $B'$  for  $\bar{B} = 0$  by  $u^{(0)}$  and  $B^{(0)}$ .

Consider small  $\bar{B}$  and put  $u' = u^{(0)} + u^{(1)}$

$$B' = B^{(0)} + B^{(1)}$$

with  $u^{(0)}$  and  $B^{(1)}$  being linear and homogeneous in  $\bar{B}$

$$\mathcal{E} = \mathcal{E}^{(0)} + \mathcal{E}(\bar{B})$$

$$\mathcal{E}^{(0)} = \overline{u^{(0)} \times B^{(0)}} \quad \leftarrow \text{no longer necessarily } = 0!$$

$$\mathcal{E}(\bar{B}) = \overline{u^{(0)} \times B^{(1)}} + \overline{u^{(1)} \times B^{(0)}}$$

$$\partial_t B' - \dots = \nabla \times (u' \times \bar{B})$$

$$\partial_t u' + \dots = \dots + f' + \frac{1}{\mu_0} (\nabla \times B') \times \bar{B} + (\nabla \times \bar{B}) \times B'$$

generates fluctuating motions

$$\partial_t B^{(1)} - \dots = \nabla \times (u^{(0)} \times \bar{B})$$

$$\partial_t u^{(1)} - \dots = \dots + \frac{1}{\mu_0} ((\nabla \times B^{(0)}) \times \bar{B} + (\nabla \times \bar{B}) \times B^{(0)})$$

$B^{(1)}$  functional of  $\bar{u}$ ,  $u^{(0)}$  and  $\bar{B}$  } both linear and homogeneous in  $\bar{B}$   
 $u^{(1)}$  functional of  $\bar{u}$ ,  $B^{(0)}$  and  $\bar{B}$  }

$$\mathcal{E}(\bar{B}) = \mathcal{E}^{(\bar{B}, u)}(\dots, u^{(0)}, \bar{B}) + \mathcal{E}^{(\bar{B}, B)}(\dots, B^{(0)}, \bar{B})$$

linear and homogeneous in  $\bar{B}$

0 6.6.2

A simple (academic) example

$$\bar{u} = 0$$

$(u^{(0)}, B^{(0)})$  homogeneous isotropic MHD turbulence

$$\underline{\underline{\mathcal{E}^{(0)} = 0}} \quad \leftarrow \text{no non-zero mean vector other than } \bar{B} \text{ available!}$$

$$\underline{\underline{\mathcal{E} = \alpha \bar{B} - \beta \nabla \times \bar{B}}}$$

Calculation of  $\alpha$  and  $\beta$  in the limit  $\eta \rightarrow 0$

$$\alpha = -\frac{1}{3} \left( \overline{u^{(0)} \cdot (\nabla \times u^{(0)})} - \frac{1}{\mu_0} \overline{B^{(0)} \cdot (\nabla \times B^{(0)})} \right) \tau_{cor} \parallel$$

$$\beta = \frac{1}{3} \overline{u^{(0)2}} \tau_{cor} \parallel$$

no » magnetic contribution « to  $\beta$ !

$B^{(0)}$  is only that part of  $B'$  which exists independent of  $\bar{B}$ !

Pouquet et al. 1976

Zeldovich et al. 1983

Vainushstein & Kichatinov 1983

o 6.6.8

More realistic cases

Considerations concerning the structure of  $\Sigma$  presented so far apply with slight modifications.

The result for  $\Sigma$  given under  
» Inhomogeneous turbulence  
influenced by the Coriolis force and a mean motion«  
applies with modified interpretations of  $g$ ,

e.g.,

$$\alpha_1^{(\Omega)}(g \cdot \Omega) \rightarrow \frac{16}{15} \left( \nabla \left( \overline{u^{(\Omega)2}} - \frac{1}{3\mu\varrho} \overline{B^{(\Omega)2}} \right) \cdot \Omega \right)$$

$$\gamma^{(0)} g \rightarrow \frac{1}{6} \nabla \left( \overline{u^{(\Omega)2}} - \frac{1}{\mu\varrho} \overline{B^{(\Omega)2}} \right) \times$$

$$\gamma^{(\Omega)} g \times \Omega \rightarrow -\frac{2}{9} \nabla \left( \overline{u^{(\Omega)2}} + \frac{1}{\mu\varrho} \overline{B^{(\Omega)2}} \right) \times \Omega$$

$$\delta^{(\Omega)} \rightarrow -\frac{2}{9} \left( \overline{u^{(\Omega)2}} - \frac{1}{\mu\varrho} \overline{B^{(\Omega)2}} \right) \times$$

$$\times \text{Equipartition } \overline{u^{(\Omega)2}} = \frac{1}{\mu\varrho} \overline{B^{(\Omega)2}}$$

$$\Rightarrow \gamma^{(0)} g = 0, \delta^{(\Omega)} = 0!$$

Rädler, Kleeorin & Rogachevskii 2003

● 6.7.

Larger mean magnetic fields,  
quenching effects

(Both cases,  $B' \rightarrow 0$  and  $B' \rightarrow \infty$  for  $\bar{B} = 0$ ,  
again admitted)

○ 6.7.1.

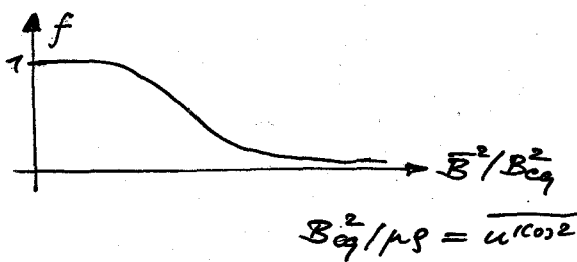
A heuristic ansatz

$$\mathcal{E} = \alpha \bar{B} - \beta \nabla \times \bar{B}$$

values for the limit  $\bar{B} \rightarrow 0$

$$\alpha = \alpha_0 f_\alpha(\bar{B}^2)$$

$$\beta = \beta_0 f_\beta(\bar{B}^2)$$



e.g.

$$f = \frac{1}{1 + c \frac{\bar{B}^2}{B_{eq}^2}}$$

What about

- other contributions to  $\mathcal{E}$   
which are nonlinear in  $\bar{B}$
- dependencies of  $\alpha$  and  $\beta$   
on derivatives of  $\bar{B}$  ?

o 6.7.2.

A simple (academic) example

$$\bar{u} = 0$$

$u'$  or  $(u', B')$  (originally) homogeneous

isotropic turbulence

$\bar{B}$  arbitrarily strong but spatial variations weak  
so that  $\bar{E}$  linear in derivatives of  $\bar{B}$

$a_{ij}, b_{ijk}$  axisymmetric tensors

w.r.t. an axis given by  $\bar{B}$ ,

independent on the sign of  $\bar{B}$

$\leadsto$

$$\begin{aligned}\bar{E} &= (\alpha - \alpha_1 (\bar{B} \cdot (\nabla \times \bar{B}))) \bar{B} \\ &\quad - (\gamma_1 \nabla \bar{B}^2 + \gamma_2 (\bar{B} \cdot \nabla) \bar{B}) \times \bar{B} \\ &\quad - \beta \nabla \times \bar{B}\end{aligned}$$

with  $\alpha, \alpha_1, \gamma_1, \gamma_2$  and  $\beta$  depending on  $\bar{B}^2$

Alternative representation

$$\begin{aligned}\bar{E} &= \alpha \bar{B} \\ &\quad - (\gamma_1 \nabla \bar{B}^2 + \gamma_2 (\bar{B} \cdot \nabla) \bar{B}) \times \bar{B} \\ &\quad - \beta \nabla \times \bar{B} - \underbrace{\beta_1 (\bar{B} \cdot (\nabla \times \bar{B})) \bar{B}}_{\alpha_1} \\ &\quad - \beta_{ij} (\nabla \times \bar{B})_j, \text{ with } \beta_{ij} = \beta \delta_{ij} + \beta_1 \bar{B}_i \bar{B}_j\end{aligned}$$

$$\left(\frac{1}{2} \nabla \bar{B}^2 - (\bar{B} \cdot \nabla) \bar{B}\right) \times \bar{B} = -\bar{B}^2 \nabla \times \bar{B} - \bar{B} \cdot (\nabla \times \bar{B}) \bar{B}$$

$\leadsto$  without loss of generality

either  $\alpha_1 = \beta_1 = 0$  or  $\gamma_1 = 0$  or  $\gamma_2 = 0$ !

o 6.2.3.

More general cases

It seems inconsequential to discuss the nonlinear dependence of  $\mathcal{E}$  on  $\bar{B}$  (i.e. the dependence of quantities like  $\alpha$  or  $\beta$  on  $\bar{B}$ ) without considering how  $\bar{u}$  depends on  $\bar{B}$ .

→ MEAN-FIELD MAGNETOFLUID DYNAMICS

• 7.

MEAN-FIELD MAGNETOFLUID DYNAMICS

• 7.1.

Basic equations

○ 7.1.1.

Starting point

For simplicity incompressible fluid,  
fluctuating motions generated by an external force

$$\partial_t \mathbf{B} = -\nabla \times (\eta \nabla \mathbf{B} - \mathbf{u} \times \mathbf{B})$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\rho(\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u}) = -\nabla p + \rho \nu \nabla^2 \mathbf{u} - 2\rho \boldsymbol{\Omega} \times \mathbf{u} + \frac{1}{\mu} (\nabla \times \mathbf{B}) \times \mathbf{B} + \mathbf{F}$$

$$\nabla \cdot \mathbf{u} = 0$$

○ 7.1.2.

Mean-field equations

$$\partial_t \bar{\mathbf{B}} = -\nabla \times (\eta \nabla \bar{\mathbf{B}} - \bar{\mathbf{u}} \times \bar{\mathbf{B}} - \underline{\underline{\mathbf{E}}})$$

$$\nabla \cdot \bar{\mathbf{B}} = 0$$

$$\underline{\underline{\mathbf{E}}} = \overline{\mathbf{u}' \times \mathbf{B}'}$$

$$\rho(\partial_t \bar{\mathbf{u}} + (\bar{\mathbf{u}} \cdot \nabla) \bar{\mathbf{u}}) = -\nabla \bar{p} + \rho \nu \nabla^2 \bar{\mathbf{u}} - 2\rho \boldsymbol{\Omega} \times \bar{\mathbf{u}} + \frac{1}{\mu} (\nabla \times \bar{\mathbf{B}}) \times \bar{\mathbf{B}} + \bar{\mathbf{F}} + \underline{\underline{\mathbf{F}'}}$$

$$\nabla \cdot \bar{\mathbf{u}} = 0$$

$$\underline{\underline{\mathbf{F}'}} = \overline{-\rho(\mathbf{u}' \cdot \nabla) \mathbf{u}'} + \frac{1}{\mu} \overline{(\nabla \times \mathbf{B}') \times \mathbf{B}'}$$

$$F_i = \frac{\partial T_{ij}}{\partial x_j}$$

$$T_{ij} = \overline{-\rho u'_i u'_j} + \frac{1}{\mu} (\overline{B'_i B'_j} - \frac{1}{2} \overline{B'^2} \delta_{ij})$$

Reynolds stresses      Maxwell stresses  
stresses due to magnetic fluctuations

0 71.3.

Properties of  $\mathcal{E}$  and  $\mathcal{F}$

$$\partial_t \mathcal{B}' = -\nabla \times (\gamma \nabla \mathcal{B}' - \bar{u} \times \mathcal{B}' - u' \times \bar{B} - u' \times \mathcal{B}' + \overline{u' \times \mathcal{B}'})$$

$$\nabla \cdot \mathcal{B}' = 0$$

$$\rho (\partial_t u' + (\bar{u} \cdot \nabla) u' + (u' \cdot \nabla) \bar{u} + (u' \cdot \nabla) u' - \overline{(u' \cdot \nabla) u'})$$

$$= -\nabla p' + \rho v \nabla^2 u' - 2\rho \mathcal{L} \times u'$$

$$+ \frac{1}{\mu} ((\nabla \times \bar{B}) \times \mathcal{B}' + (\nabla \times \mathcal{B}') \times \bar{B} + (\nabla \times \mathcal{B}') \times \mathcal{B}' - \overline{(\nabla \times \mathcal{B}') \times \mathcal{B}'})$$

$$+ F'$$

$$\nabla \cdot u = 0$$

~

$\mathcal{B}', u'$  are functionals of  $\bar{B}, \bar{u}$  and  $F'$

~

$\mathcal{E}, \mathcal{F}$  are functionals of  $\bar{B}, \bar{u}$  and  $F'$

Assume that  $F'$  independent of  $\bar{B}$  and  $\bar{u}$ .

Denote  $\mathcal{B}'$  and  $u'$  for  $\bar{B} = \bar{u} = 0$  by  $\mathcal{B}'^{(0)}$  and  $u'^{(0)}$  and express  $F'$  by these quantities.

~

$\mathcal{E}, \mathcal{F}$  are functionals of  $\bar{B}, \bar{u}, \mathcal{B}'^{(0)}$  and  $u'^{(0)}$

As for  $\mathcal{E}$  see above.



● 8.

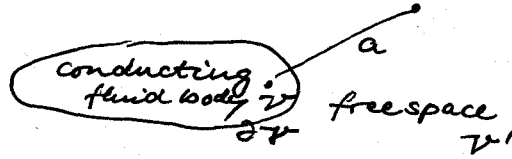
KINEMATIC MEAN-FIELD DYNAMO MODELS

● 8.1

Basic equations

○ 8.1.1.

Starting point



$$\nabla \times (\eta \nabla \times \mathbf{B} - \mathbf{u} \times \mathbf{B}) + \partial_t \mathbf{B} = 0 \quad \left. \vphantom{\nabla \times (\eta \nabla \times \mathbf{B} - \mathbf{u} \times \mathbf{B}) + \partial_t \mathbf{B} = 0} \right\} \text{ in } V$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\left. \begin{aligned} \nabla \times \mathbf{B} &= 0 \\ \nabla \cdot \mathbf{B} &= 0 \end{aligned} \right\} \text{ in } V'$$

$$[\mathbf{B}] = 0 \text{ across } \partial V$$

$$\mathbf{B} \rightarrow 0 \text{ as } a \rightarrow \infty$$

○ 8.1.2.

Mean-field equations

$$\nabla \times (\eta \nabla \times \bar{\mathbf{B}} - \bar{\mathbf{u}} \times \bar{\mathbf{B}} - \underline{\underline{\mathcal{E}(\bar{\mathbf{B}})}}) + \partial_t \bar{\mathbf{B}} = 0 \quad \left. \vphantom{\nabla \times (\eta \nabla \times \bar{\mathbf{B}} - \bar{\mathbf{u}} \times \bar{\mathbf{B}} - \underline{\underline{\mathcal{E}(\bar{\mathbf{B}})}}) + \partial_t \bar{\mathbf{B}} = 0} \right\} \text{ in } V$$

$$\nabla \cdot \bar{\mathbf{B}} = 0$$

$$\left. \begin{aligned} \nabla \times \bar{\mathbf{B}} &= 0 \\ \nabla \cdot \bar{\mathbf{B}} &= 0 \end{aligned} \right\} \text{ in } V'$$

$$[\bar{\mathbf{B}}] = 0 \text{ across } \partial V$$

$$\bar{\mathbf{B}} \rightarrow 0 \text{ as } a \rightarrow \infty$$

↑ to be specified

» MEAN-FIELD DYNAMO «:  $\bar{\mathbf{B}} \rightarrow$  as  $t \rightarrow \infty$

- Existence of a »mean-field dynamo« implies the existence of a dynamo (as discussed before).
- Mean fields are not subject to Cowling's theorem (unless  $\mathcal{E} \cdot \bar{\mathbf{B}} = 0$ ).
- Magnetic energy balance

$$\frac{d}{dt} \int_V \frac{\bar{\mathbf{B}}^2}{2\mu} dv = - \int_V \frac{\bar{\mathbf{j}}^2}{\sigma} dv - \int_V \bar{\mathbf{u}} \cdot (\bar{\mathbf{j}} \times \bar{\mathbf{B}}) dv + \int_V \bar{\mathbf{j}} \cdot \bar{\mathcal{E}} dv$$

energy stored in the mean magnetic field

● 8.2.

» Traditional assumptions  
and consequences

○ 8.2.1.

Assume that

the shape of the fluid body  
and the distribution of  $\eta$   
are

- symmetric about the rotation axis
- symmetric about the equatorial plane
- constant in time

Assume also that

all mean quantities depending on  $u (= \bar{u} + u')$   
are invariant under

- rotation of  $u$  about the rotation axis
- reflexion of  $u$  about the equatorial plane
- time shift in  $u$

Simple consequences

- $\bar{u} = \bar{u}_{mer} + \bar{u}_{rot}$

$\bar{u}_{mer}$  and  $\bar{u}_{rot}$  symmetric about  
rotation axis and equatorial plane  
and steady

- $\overline{u' \cdot (\nabla \times u')}$   
symmetric about rotation axis,  
antisymmetric about equatorial plane  
and steady

o 8.2.2.

Then any solution  $\bar{B}$  has the form,  
or is a superposition of solutions of the form,

$$\bar{B} = \text{Re}(\bar{B} \exp(im\varphi + pt))$$

$$p = \lambda + i\omega \quad \lambda, \omega \text{ real}$$

- symmetric about rotation axis
- antisymmetric  $A_m$   
or symmetric  $S_m$  } modes  
about equatorial plane
- steady

DYNAMO:  $\lambda \geq 0$

$\omega = 0$  monotonous

$\omega \neq 0$  oscillatory dependence on time

If  $\omega \neq 0$

- axisymmetric ( $m = 0$ ) modes

intrinsically oscillatory

- non-axisymmetric ( $m \neq 0$ ) modes

waves traveling with angular velocity

$$\dot{\varphi} = -\omega/m,$$

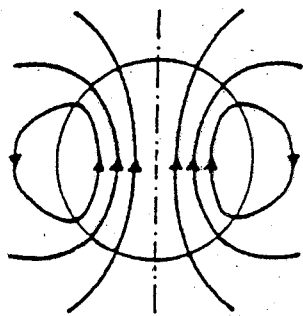
in a proper frame of reference steady

o 8.2.3.

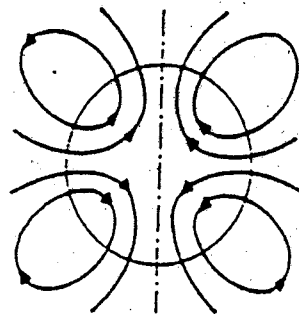
Assume finally

$$\bar{E} = -\alpha \cdot \bar{B} - \gamma \times \bar{B}$$

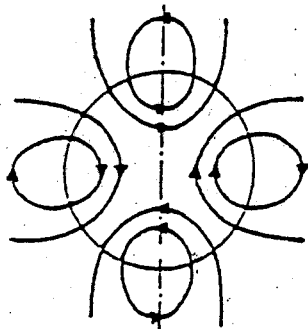
$$- \beta \cdot \nabla \times \bar{B} - \delta \times (\nabla \times \bar{B}) - \kappa \cdot (\nabla \bar{B})^{(s)}$$



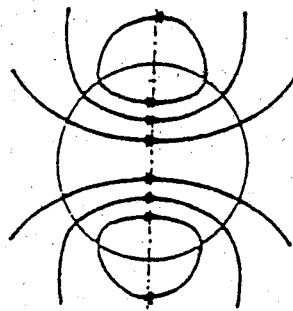
A0



S0



A1



S1

● 2.3.

Basic dynamo mechanisms

○ 2.3.1

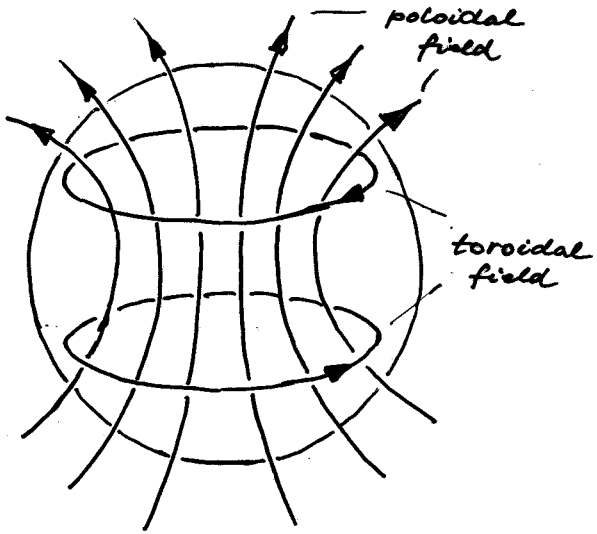
In all cases investigated so far

interplay

between the poloidal and toroidal parts  
of the magnetic field:

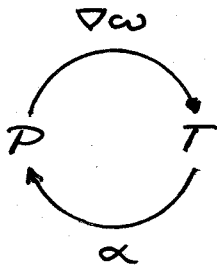


$\alpha$ -effect dynamo models

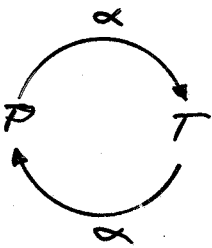


$\alpha < 0$

$\alpha > 0$



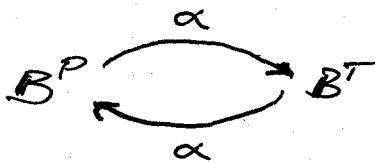
$\alpha\omega$  - model



$\alpha^2$  - model

o 8.3.2.

$\alpha^2$ -mechanism



$$|B^P| \approx |B^T|$$

Steenbeck & Krause 1969

Roberts 1972

Roberts & Stix 1972

Rädler 1975, 1979, 1986

Busse 1979

Busse & Mein 1979

Rüdiger 1980

⋮

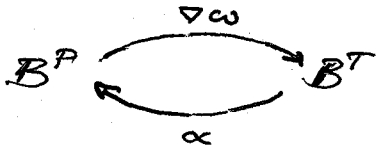
Excitation conditions for A0, S0, A1 and S1 modes  
very close together

A0 and S0 modes in general non-oscillatory

Anisotropies of the  $\alpha$ -effect lead to preferences  
of non-axisymmetric magnetic fields

o 8.3.3.

$\alpha\omega$ -mechanism



$$|B^P| \ll |B^T|$$

Steenbeck & Krause 1969

Deinzer & Stix 1971

Stix 1971, 1973, 1976

Levy 1972

Roberts & Stix 1972

Köhler 1973

Ivanova & Ruzmaikin 1976

Yoshimura 1979

Rädler 1986

Schmidt 1987

Brandenburg 1988

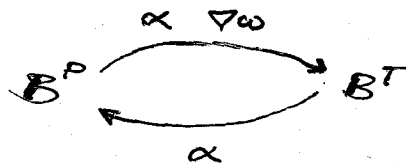
⋮

One of the axisymmetric modes (AO or SO)  
clearly preferred over all other modes.

Axisymmetric modes can be oscillatory  
or non-oscillatory (depending, e.g.,  
on the signs of  $\alpha$  and  $\partial\omega/\partial r$ ).

Oscillatory behaviour includes equatorward  
or poleward migration of toroidal  
field belts (dynamo waves).

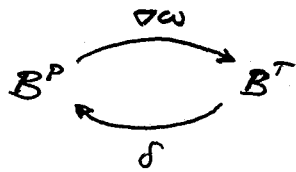
$\alpha^2\omega$ -mechanism





o 8.3.4.

$\delta\omega$ -mechanism



Rädler 1969, 1970,  
1976, 1986

Roberts & Stix 1976

Stix 1976

$$E = \dots - \int^{(\Omega)} \Omega \times (\nabla \times \bar{B})$$

$$- \int^{(\omega)} \omega \times (\nabla \times \bar{B}) \dots$$

$$\uparrow = \nabla \times \bar{u}$$

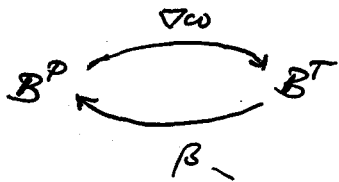
No  $\delta^2$ -mechanism

- see magnetic energy balance,

$$\bar{j} \cdot (-\Omega \times \bar{j}) = \bar{j} \cdot (\omega \times \bar{j}) = 0$$

o 8.3.5

$\beta_{\Omega}$ -mechanism



Rädler 1986

$\beta_{\Omega}$   
special components  
of the  $\beta$  tensor  
depending on  $\Omega$